

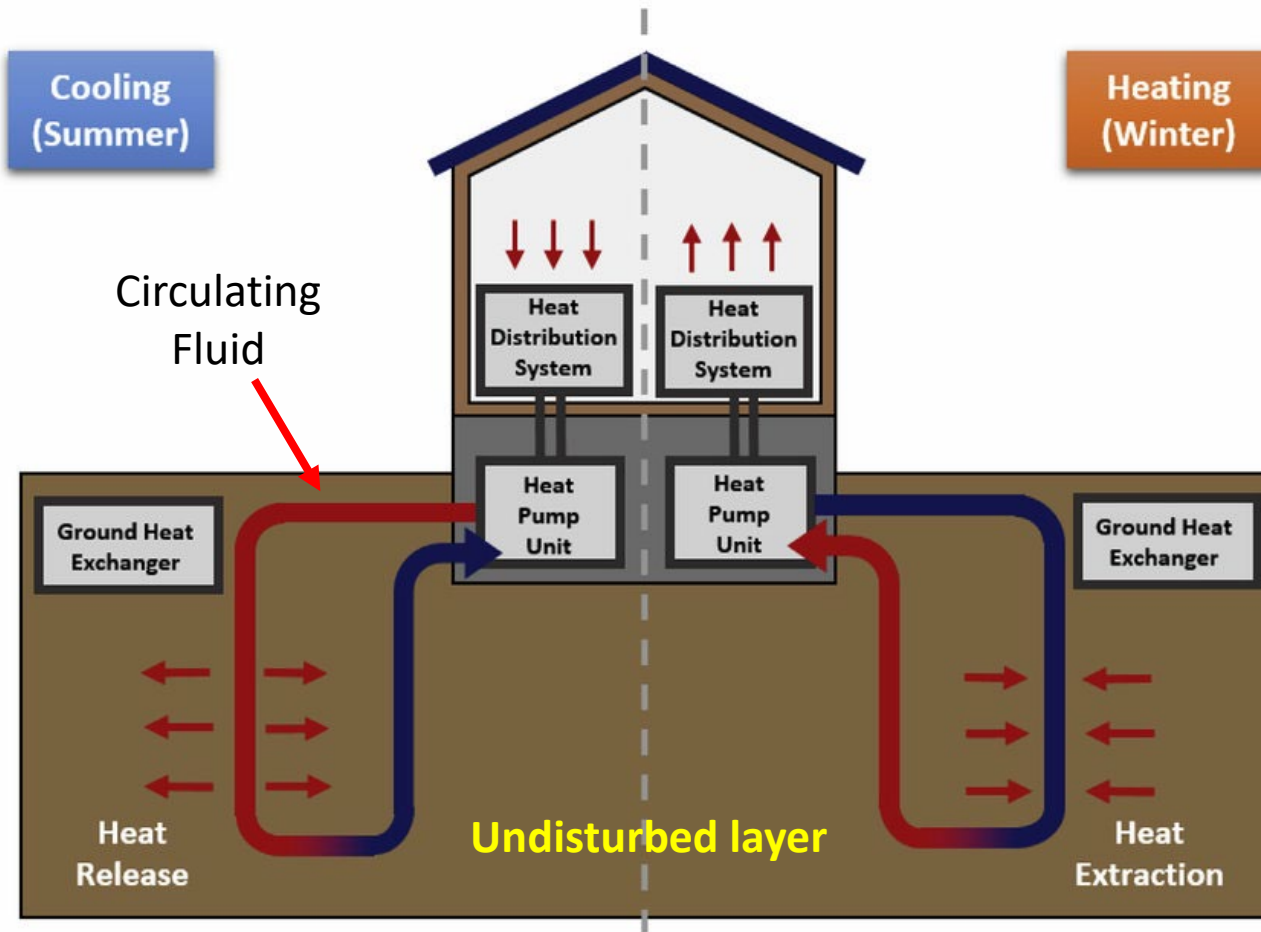
Development and application of a new calculation method for double spiral ground heat exchangers

Kunning Yang*, Takao Katsura, Katsunori Nagano
Hokkaido University

- Background
- Development of Simulation Tool
- Validation
- Problem & Discussion
- Conclusion



Ground Source Heat pump (GSHP) System



Undisturbed layer :

- constant temperature throughout a year
- 1-3°C higher than annual mean temperature

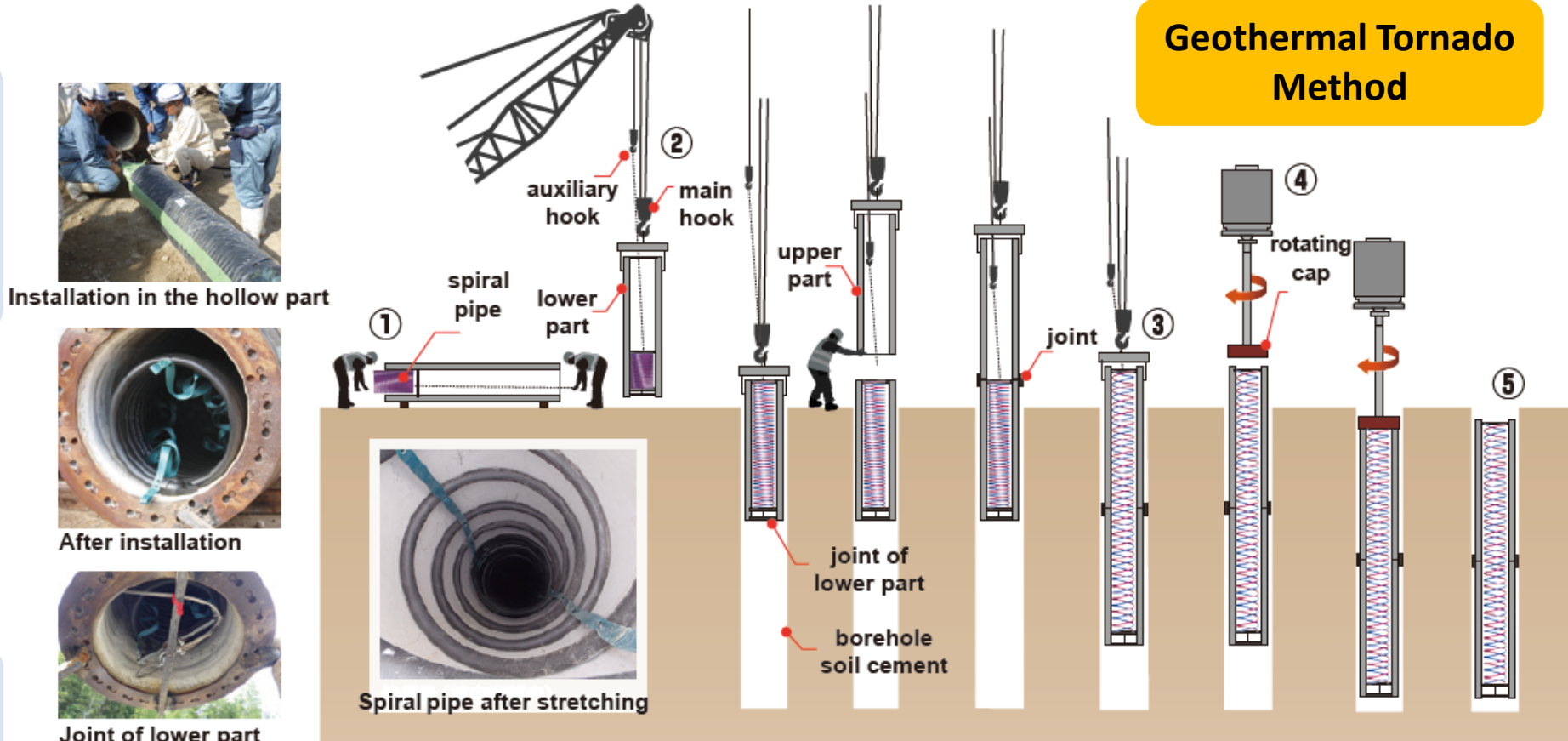
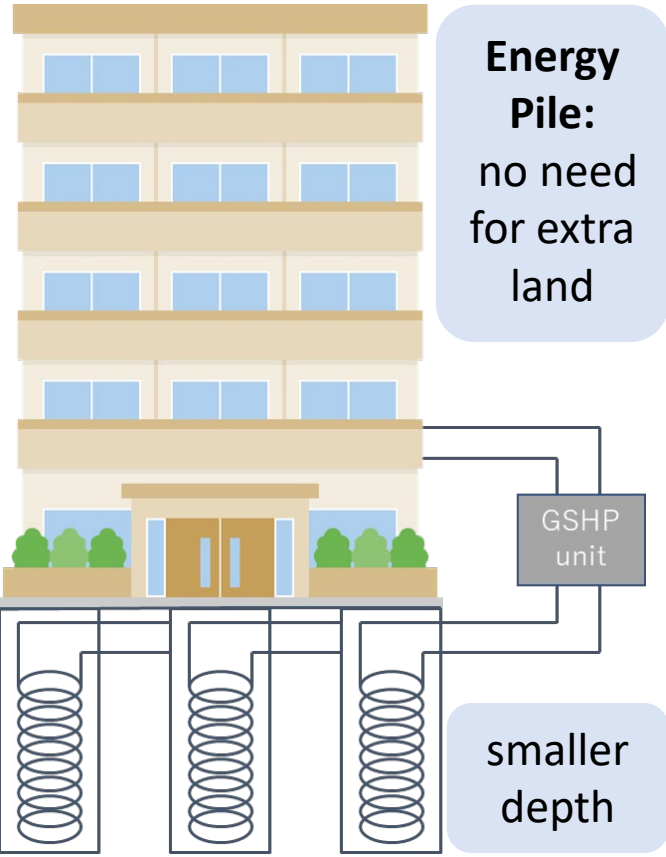
Advantages :

1. Reliable heat source
2. Higher efficiency
3. Not intermittent
4. Less maintenance

Disadvantages :

1. Large site area required to install GHEs
2. high installation cost for drilling

Geothermal Tornado Method



<http://www.japanpile.co.jp/method/pdf/tornado.pdf>

Installation of spiral GHE

①



②



③



④



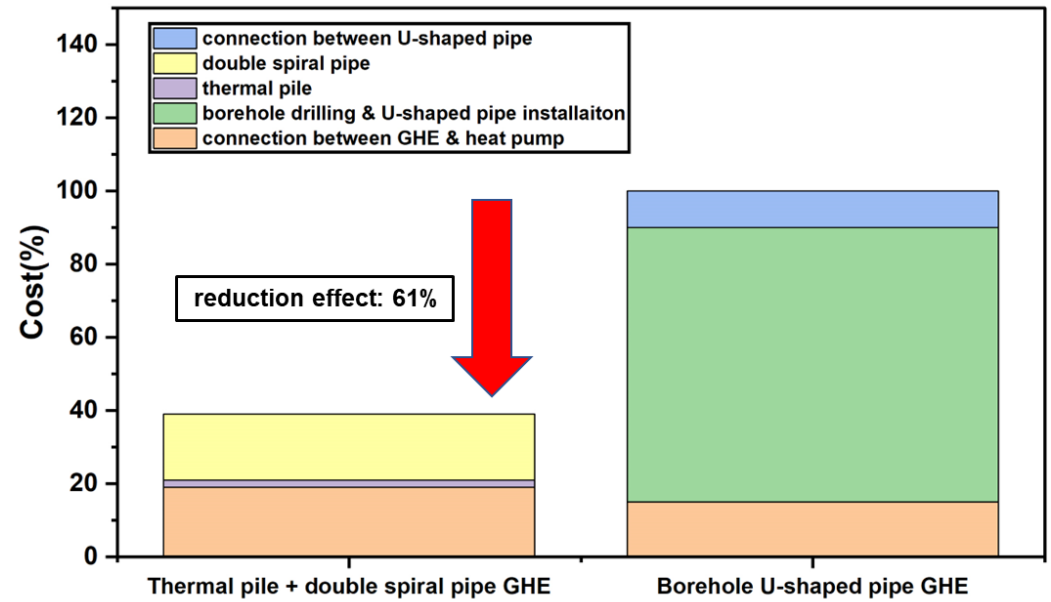
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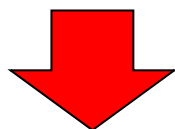
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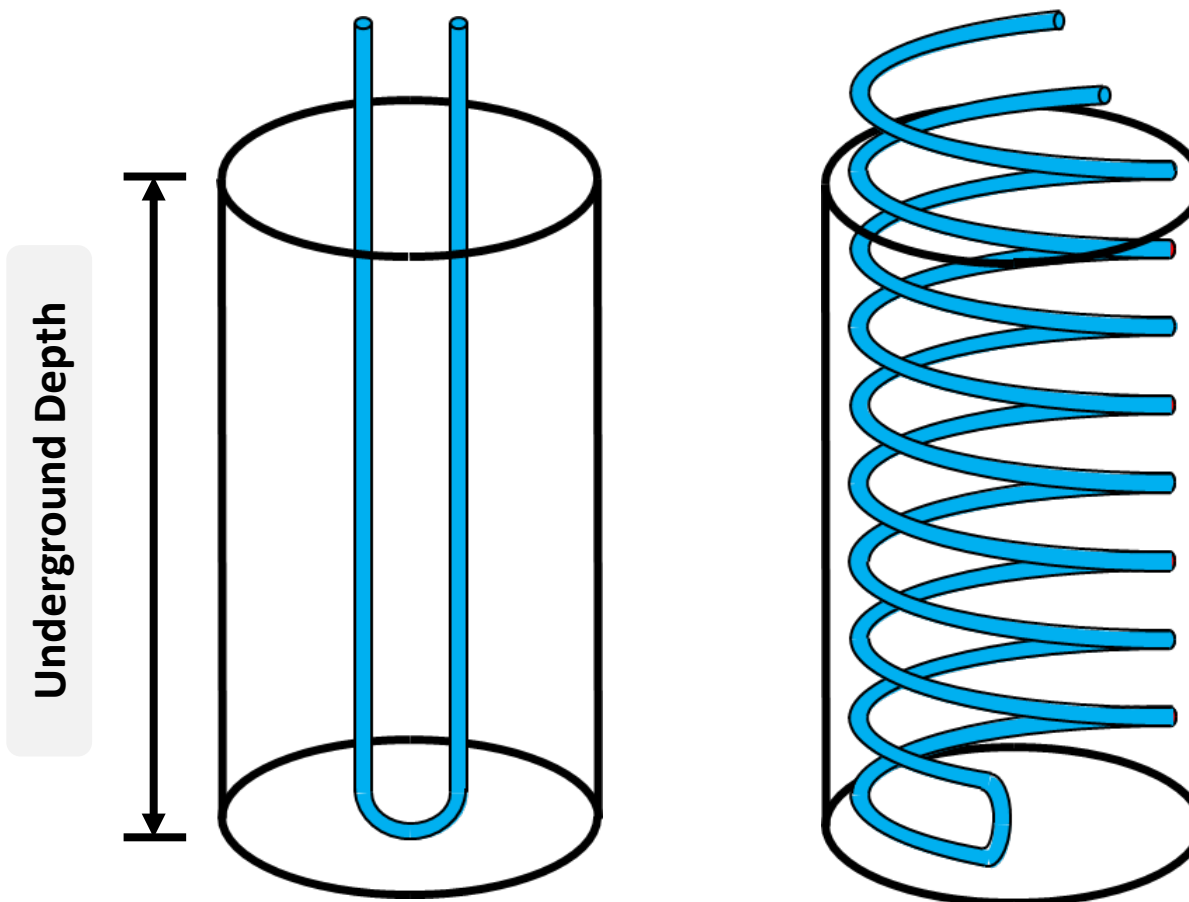
Drilling Work:
100 m (U-tube)
↓
20 m (spiral tube)

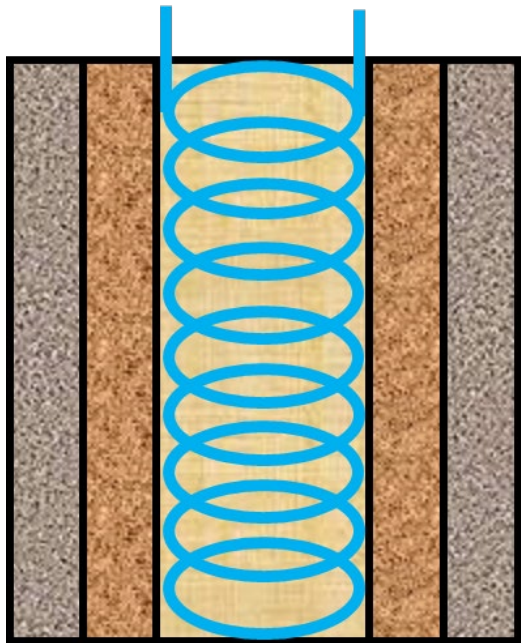


Spiral tube has **longer length** than conventional U-tube

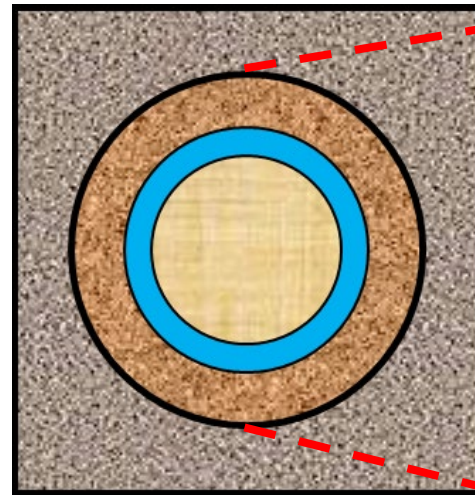


Larger heat transfer area between ground and circulating fluid

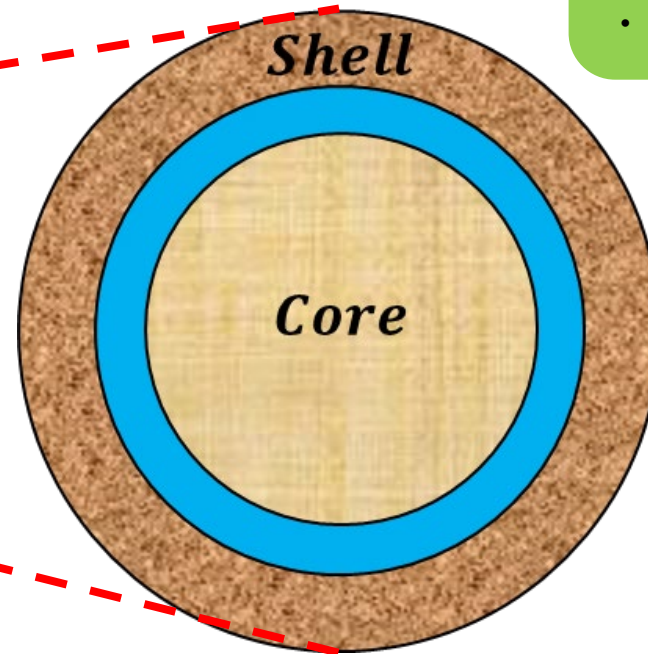




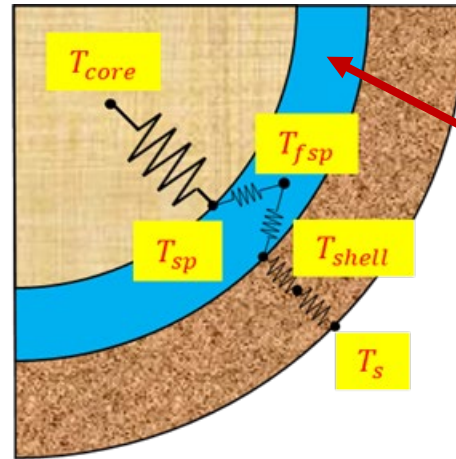
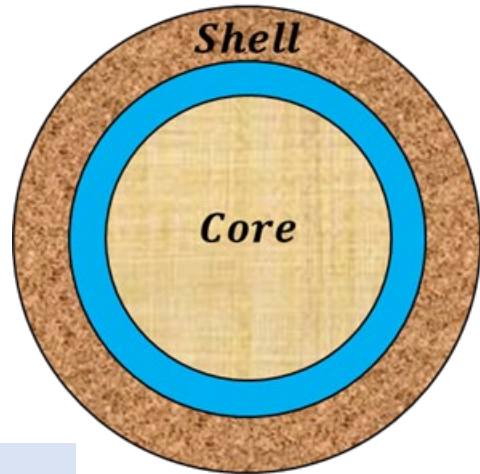
Sectional view



Top view



- 3 parts:**
- pile material (shell)
 - spiral tube
 - grout material (core)

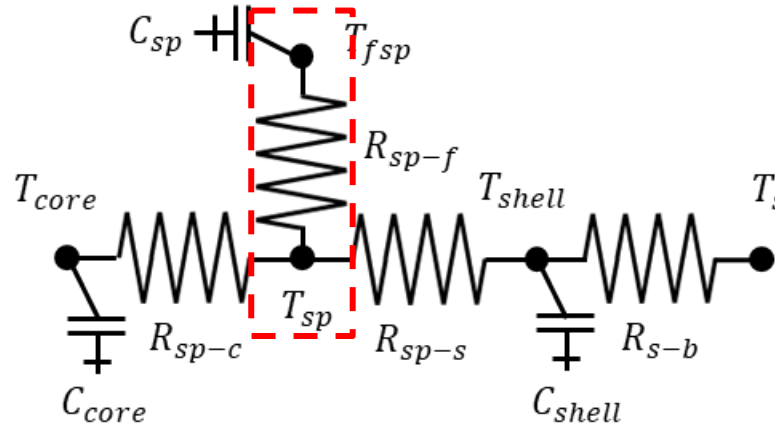


Spiral pipe (small diameter) can be neglected and simplified to a **line heat source/ heat sink**

Summer: inject heat to ground
Winter: extract heat from ground

Capacity Resistance Model

lumped thermal capacity model
• transient heat conduction approach

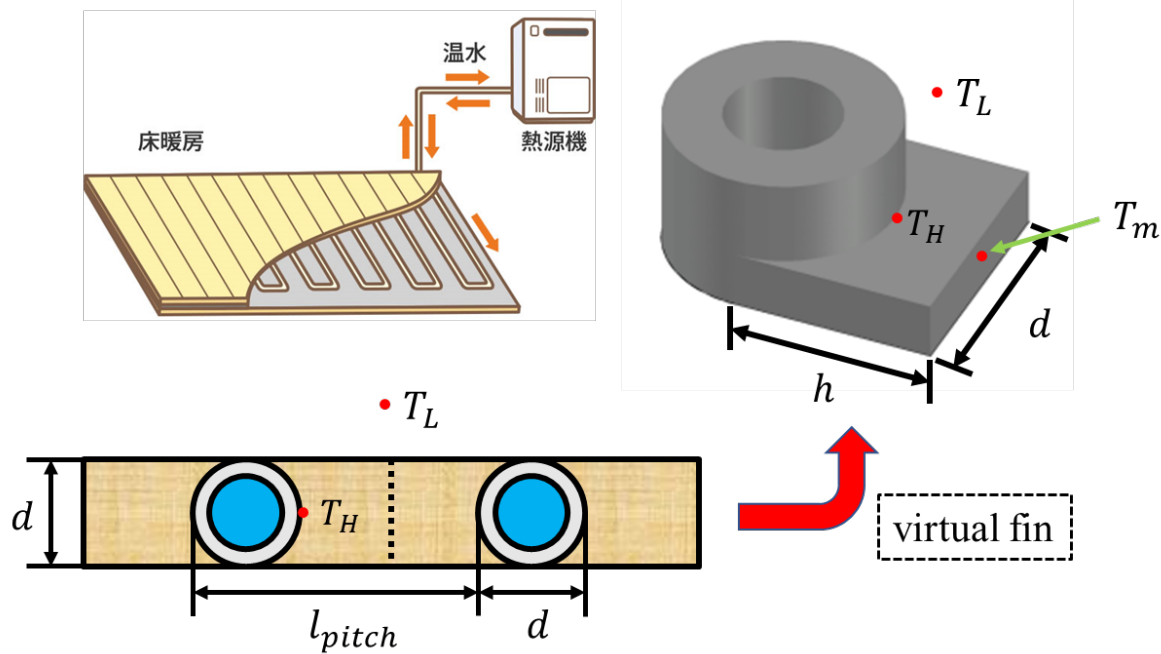


Heat transfer inside energy pile



One-dimension heat conduction in multilayer cylindrical wall

Zarella, A. & de Carli, M. Heat transfer analysis of short helical borehole heat exchangers. Applied Energy 102, (2013).



Kollmar-Liese model

For hot water floor heating system, in the floor, a virtual fin is assumed

The mean temperature of the virtual fin:

$$T_m = T_L + \eta \times (T_H - T_L)$$

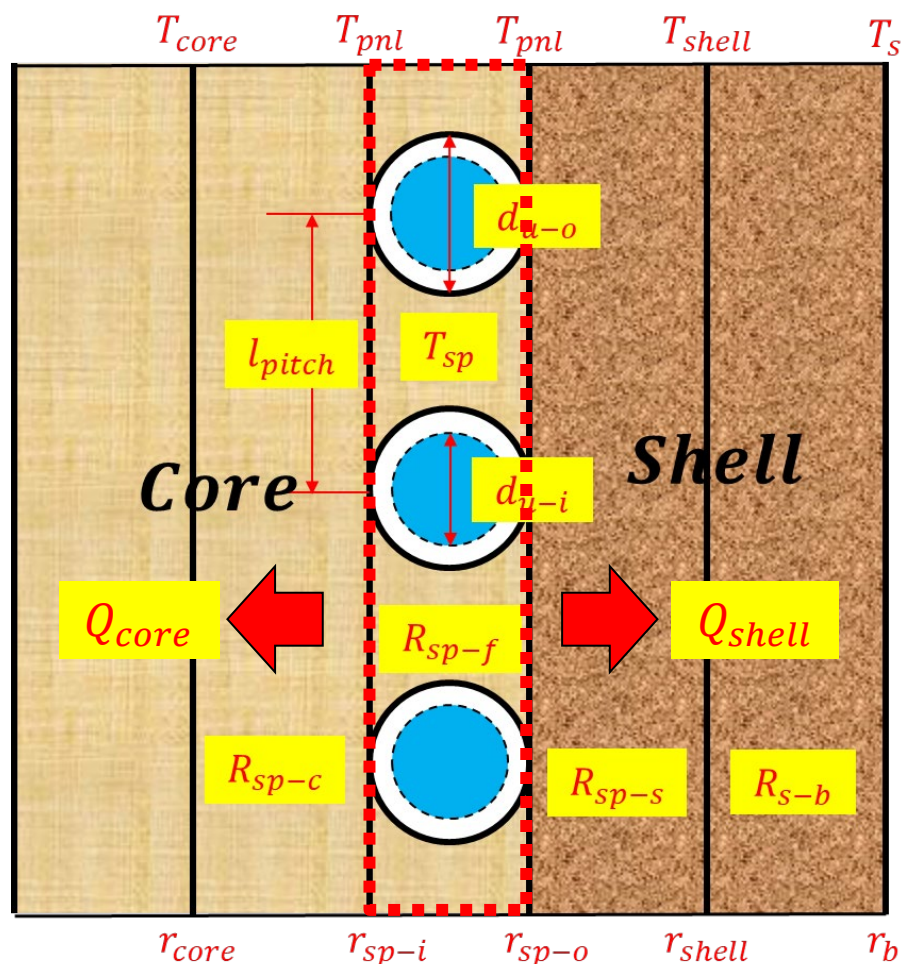
Heat transfer rate from floor to air:

$$Q = \alpha \times \eta \times (T_H - T_L) \\ = \alpha \times (T_m - T_L)$$

The heat transfer coefficient (fin efficient):

$$m = \sqrt{\frac{2\alpha}{\lambda d}}; h = \frac{1}{2} \times (l_{pitch} - d); \eta = \frac{\tanh(mh)}{mh}$$

Ishino, H. "Research on Calculation Method of Thermal Design Load in Radiant Heating and Cooling Systems." Sixth International IBPSA Conference (BS' 99). 885-892 (1999).



Layer between "core" and "shell" is considered as a "vertical" floor panel.

By analogy, temperature of the "panel" T_{pnl} :

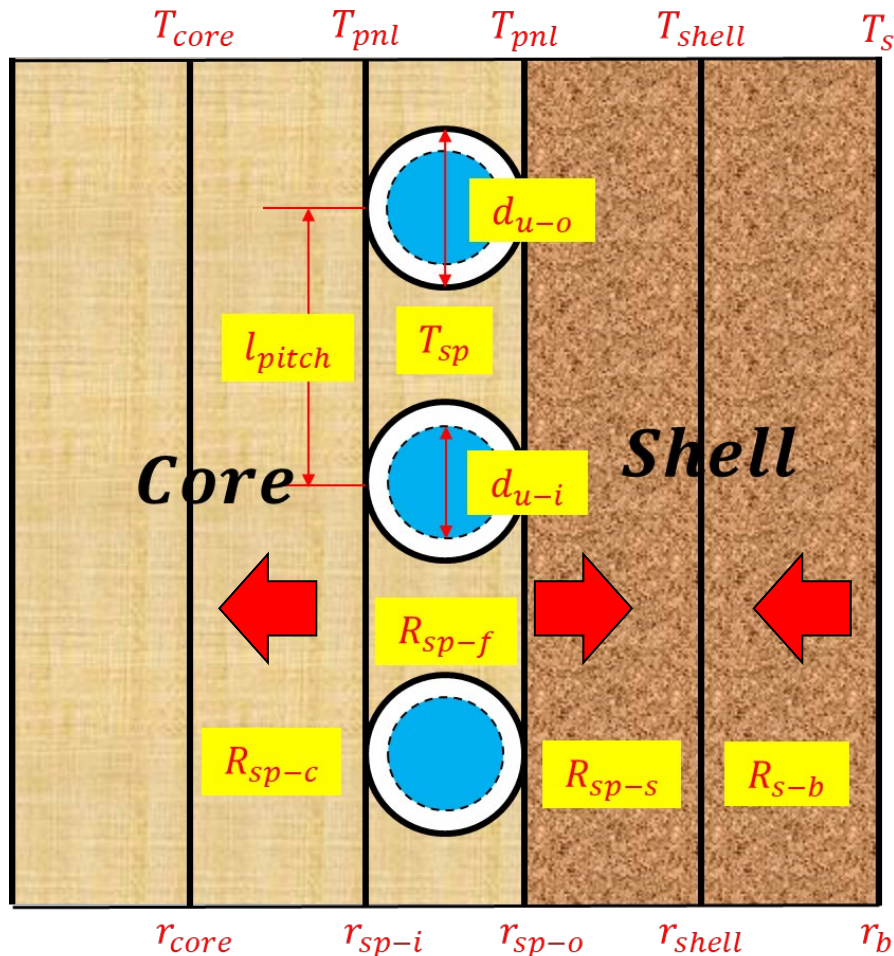
$$T_{pnl} = T_{core} + \eta_{core} \times (T_{sp} - T_{core})$$

$$T_{pnl} = T_{shell} + \eta_{shell} \times (T_{sp} - T_{shell})$$



$$T_{pnl} = \frac{1}{2} \times [(T_{sp} - T_{core})\eta_{core} + T_{core}]$$

$$+ \frac{1}{2} \times [(T_{sp} - T_{shell})\eta_{shell} + T_{shell}]$$



Thermal resistance between spiral tube surface and circulating fluid:

$$R_{sp-f} = \frac{1}{2\pi \times r_{u-i} \times l_{sp} \times \alpha_f} + \frac{1}{2\pi \times \lambda_p \times l_{sp}} \times \ln\left(\frac{r_{u-o}}{r_{u-i}}\right)$$

Heat balance in

• spiral tube:

$$c_f \rho_f V_{sp} \frac{dT_{fu}}{dt} = c_f \rho_f L V_f (T_{p-in} - T_{p-out}) + \frac{T_{sp} - T_{fsp}}{R_{sp-f}}$$

• core:

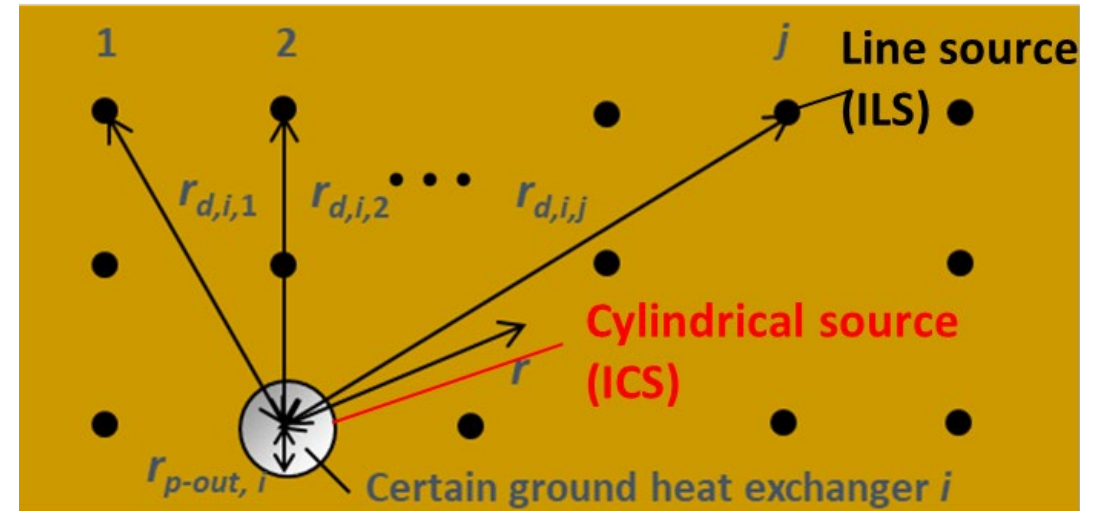
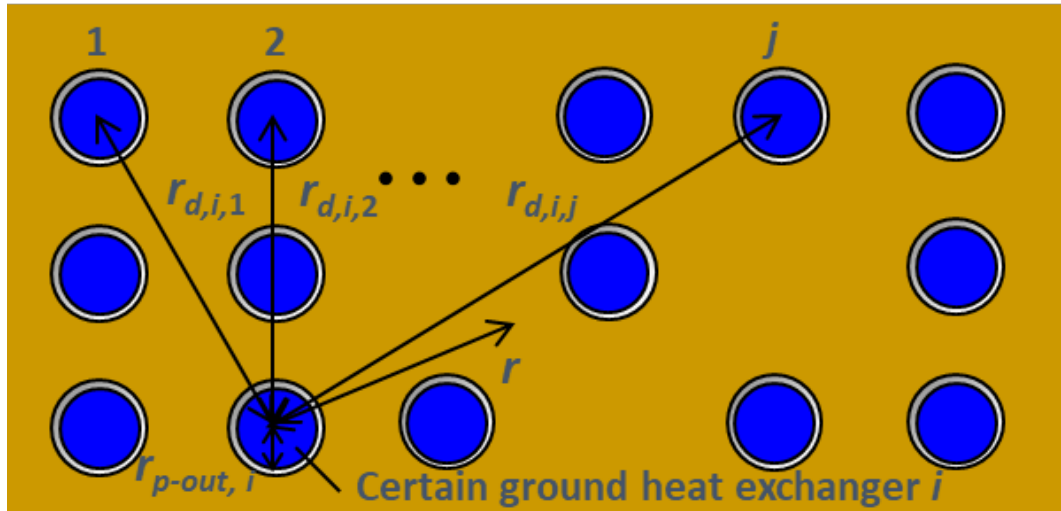
$$c_g \rho_g V_{core} \frac{dT_{core}}{dt} = \frac{1}{R_{sp-c}} (T_{pnl} - T_{core})$$

• shell:

$$c_g \rho_g V_{shell} \frac{dT_{shell}}{dt} = \frac{1}{R_{sp-s}} (T_{pnl} - T_{shell}) + \frac{T_s - T_{shell}}{R_{s-b}}$$



GroundClub (GSHP system simulation program)



Infinite cylindrical source

Infinite line source

$$\Delta T_{s,i}(r_{p-out,i}, t) = \Delta T_{s,i,i}(r_{p-out,i}, t) + \sum_{j=1}^m \Delta T_{s,i,j}(r_{d,i,j}, t)$$

Temperature change of the considered GHE

Temperature change of the neighboring GHE

- Calculation of ground temperature change
- simplified & fast speed
 - accurate

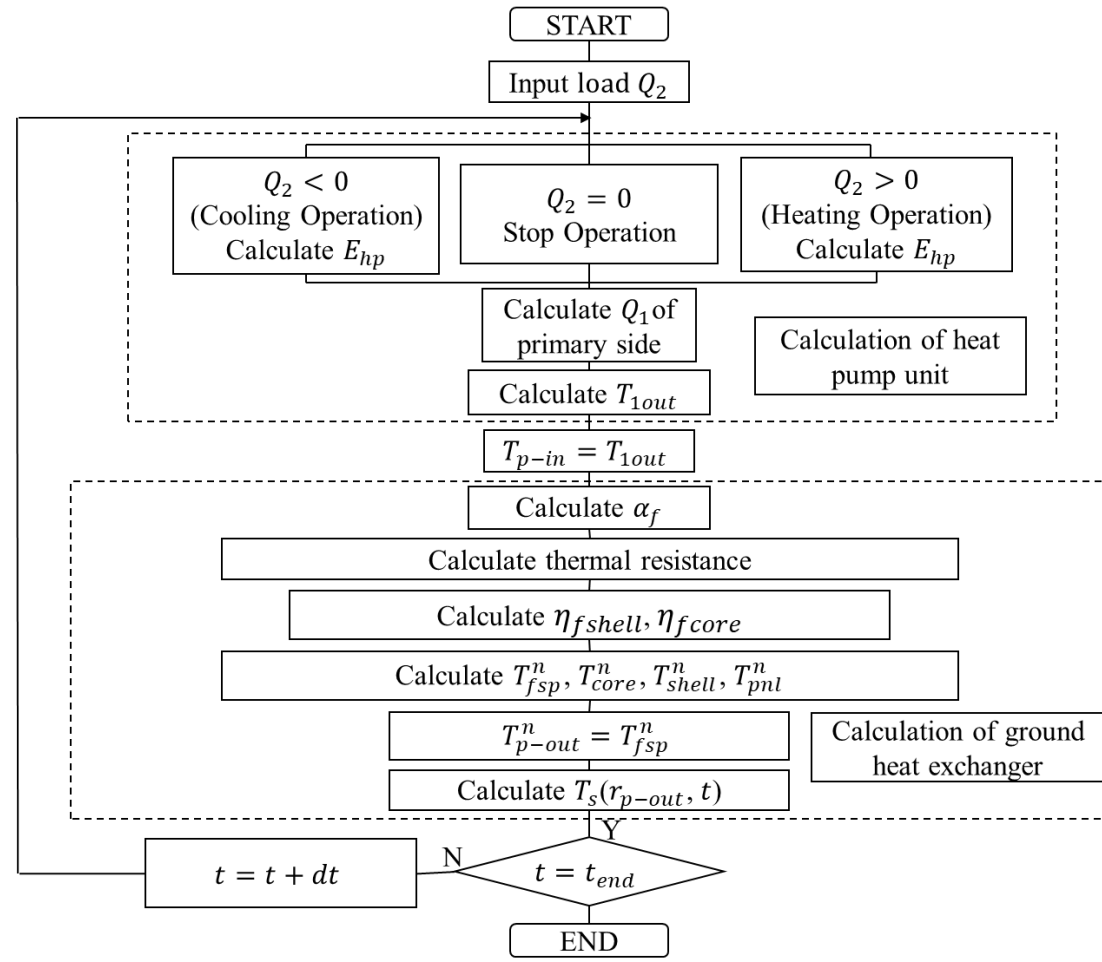
Input: building data, specifications of heat pump and ground heat exchanger, soil data, etc.

Output: pipe inlet/outlet temperature; ground temperature

Platform: MATLAB

Inside borehole (energy pile):
New calculation method

Outside borehole (ground):
GroundClub



M's Industry Group	
Building	<ul style="list-style-type: none"> • Location: Sapporo, Japan • Floor area: 650.85 m² • Number of floors: 3 • Nearly ZEB verified • Operation time: 2021/7 ~
ZEB technology	<ul style="list-style-type: none"> • GSHP system • Total heat exchange ventilation system • PV system • Radiant air conditioning system
PHC energy pile	<ul style="list-style-type: none"> • Outer diameter: 600 mm • Depth: 20 m • Pile material: concrete
Spiral GHE	<ul style="list-style-type: none"> • Diameter: 400 mm • Pipe outer diameter: 32 mm • Pipe inner diameter: 26 mm • Pitch: 250 mm

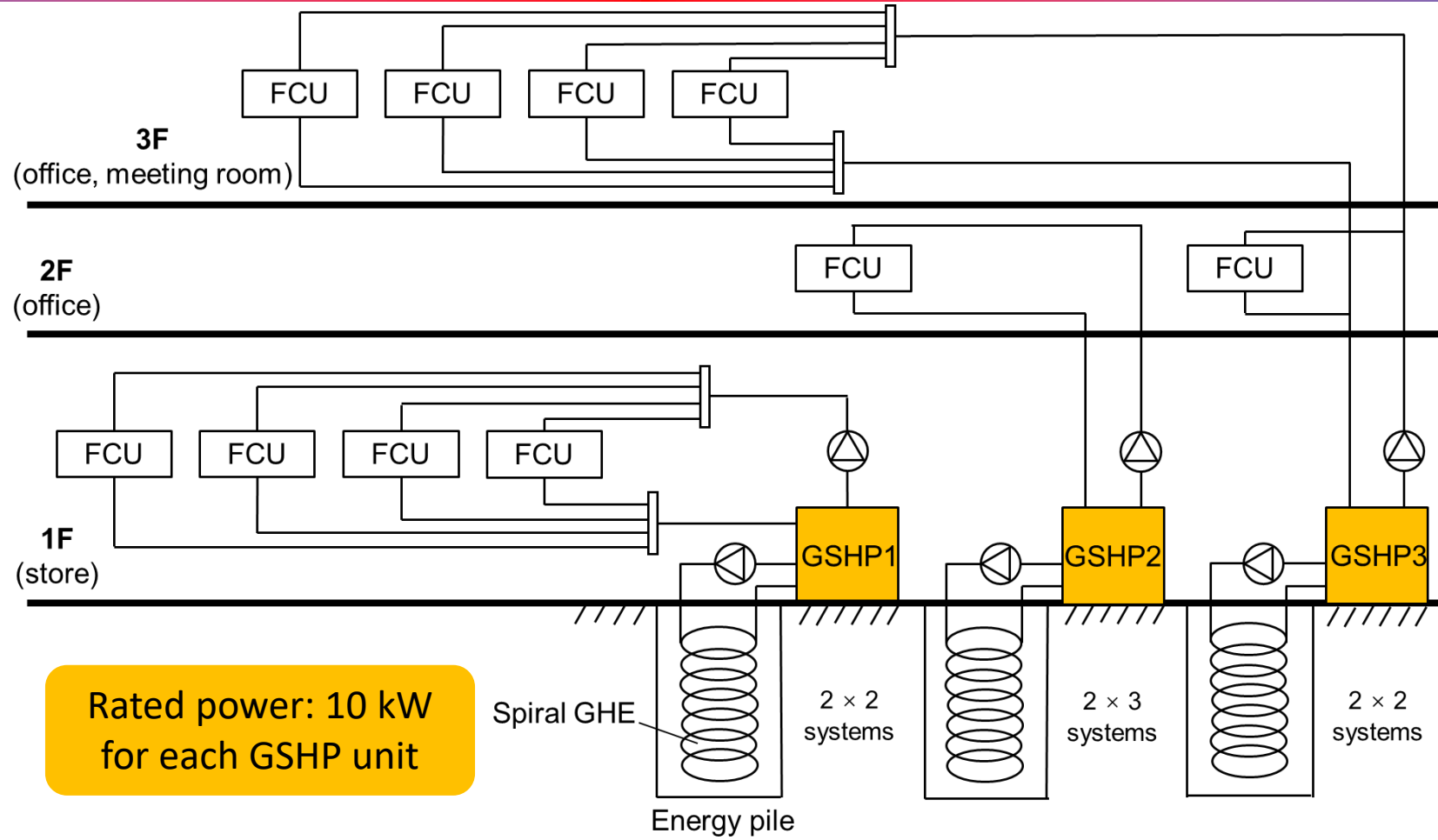




Building Overview



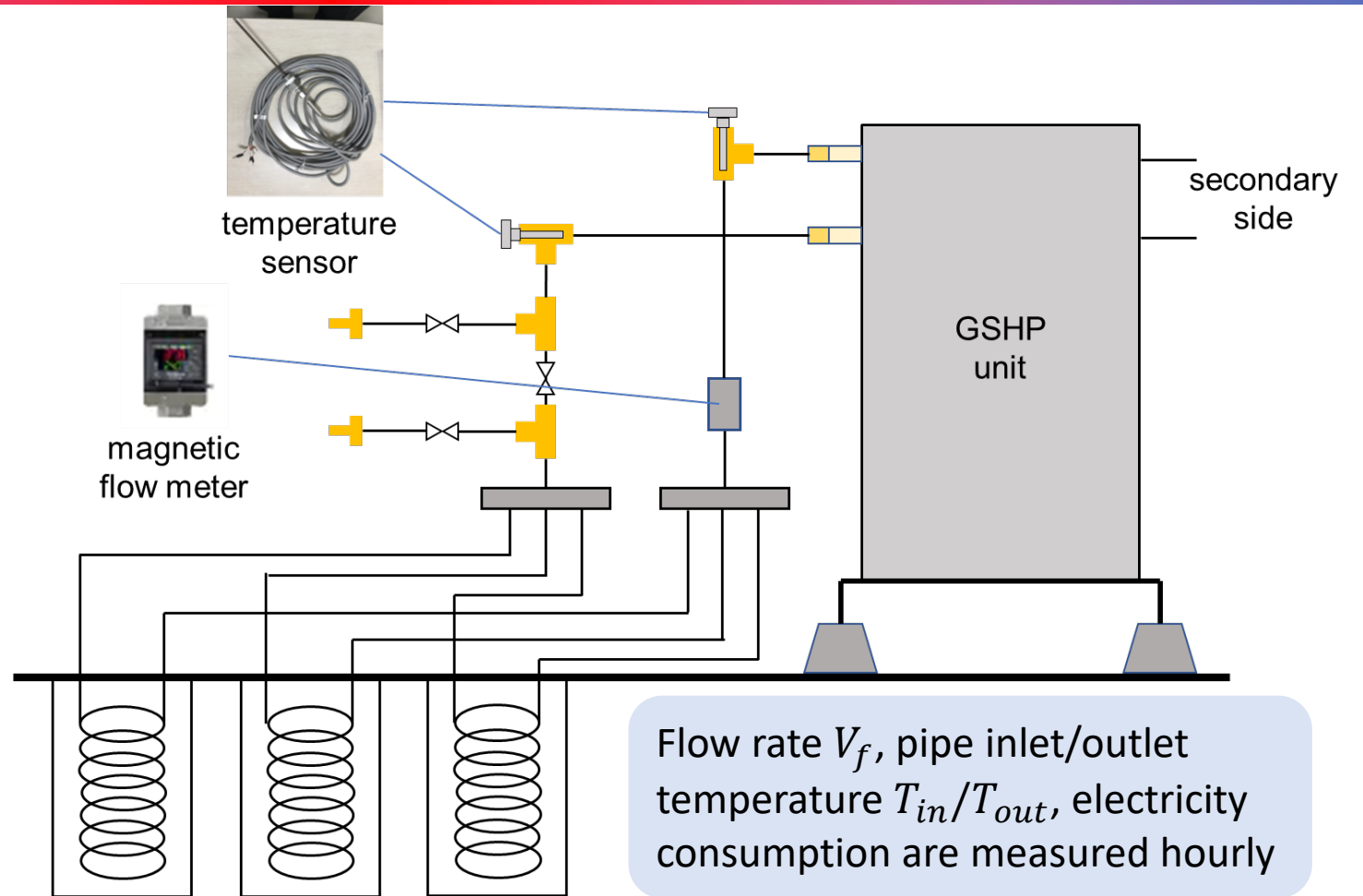
Longest operating time



Rated power: 10 kW for each GSHP unit



GSHP units in 1st floor



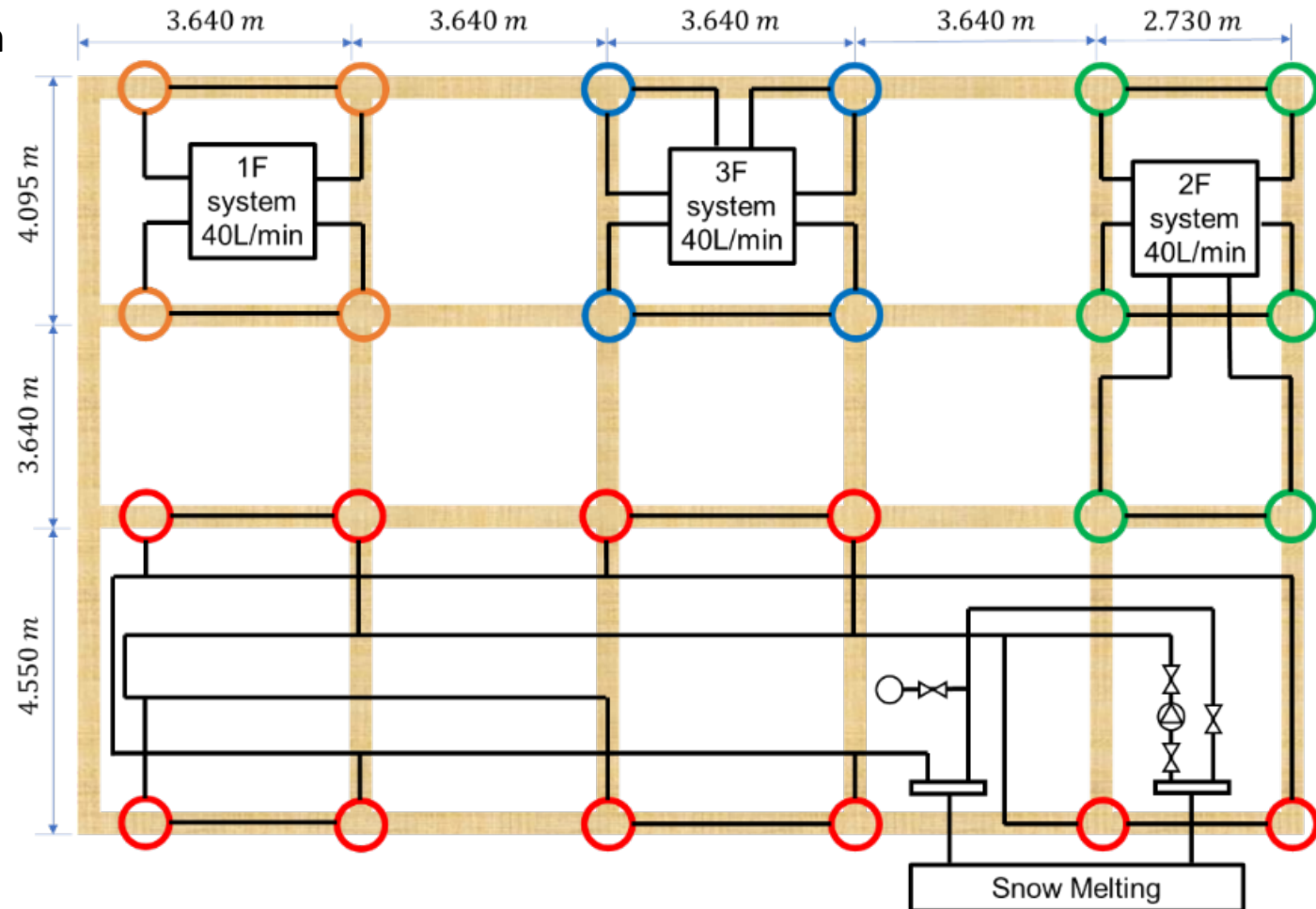
24 thermal piles installed on each floor of the house

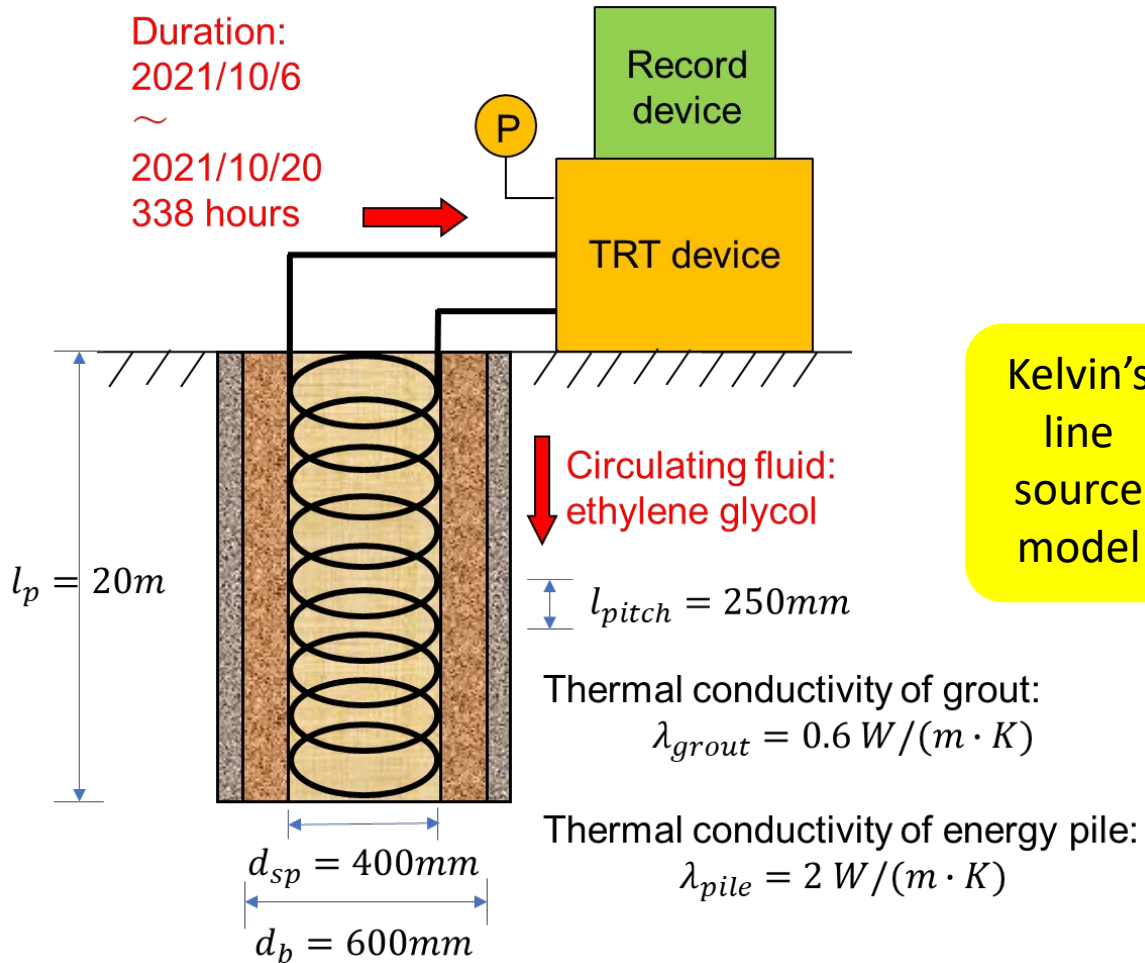
- **1st Floor:**
 - 4 (2 series × 2 parallel)

- **2nd Floor:**
 - 6 (2 series × 3 parallel)

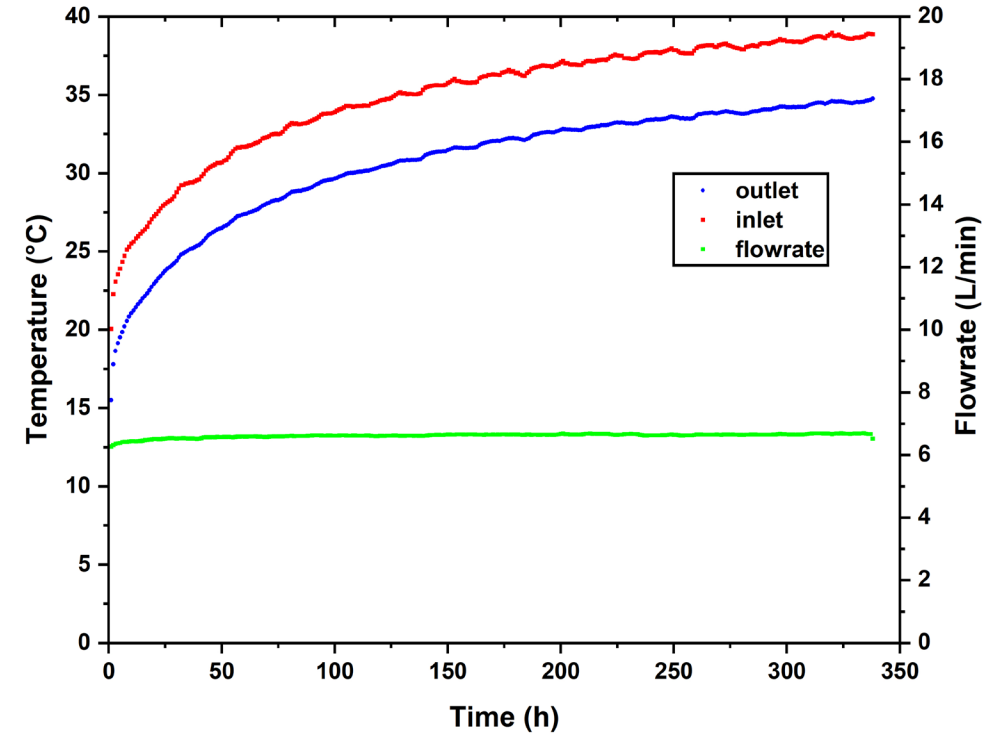
- **3rd Floor:**
 - 4 (1 + 1 + 2)

- **Snow melting: 10**





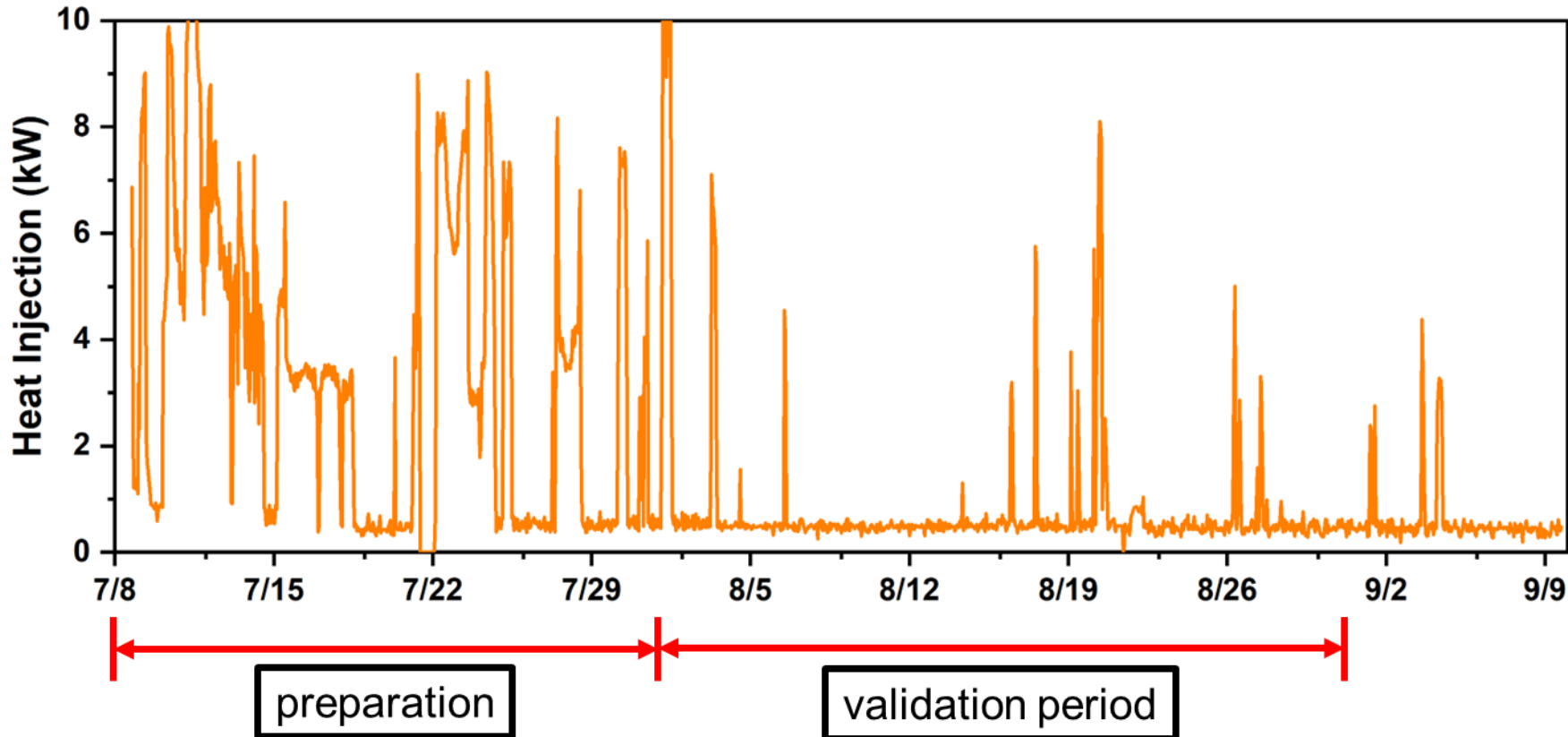
Kelvin's
line
source
model



Effective thermal conductivity of ground soil:
 $\lambda_a = 1.846 [W/m \cdot K]$ (used for simulation)



Space cooling operation (summer)



Time period:
2021/8/1 ~ 2021/8/31

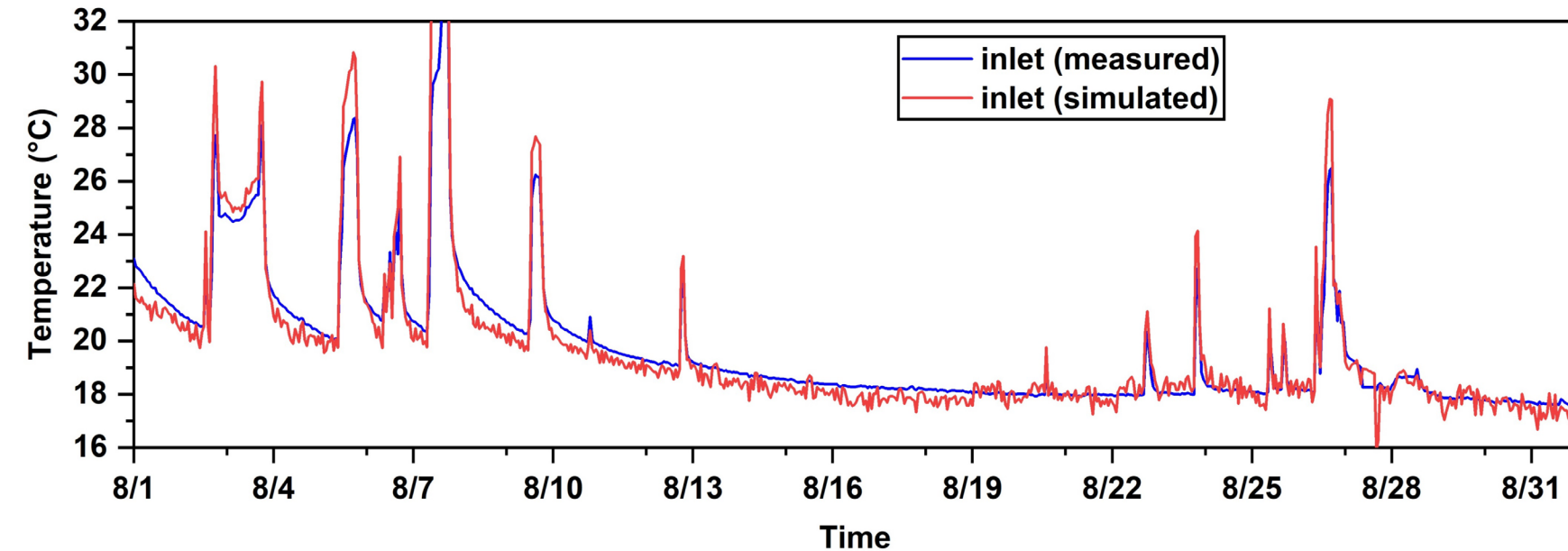
Heat injection to the ground
(primary load):

$$Q = \rho_f c_f V_f (T_{in} - T_{out})$$

long-term operation at low
load



Space cooling operation (summer)



Initial ground temperature: 12 °C

For pipe inlet temperature:

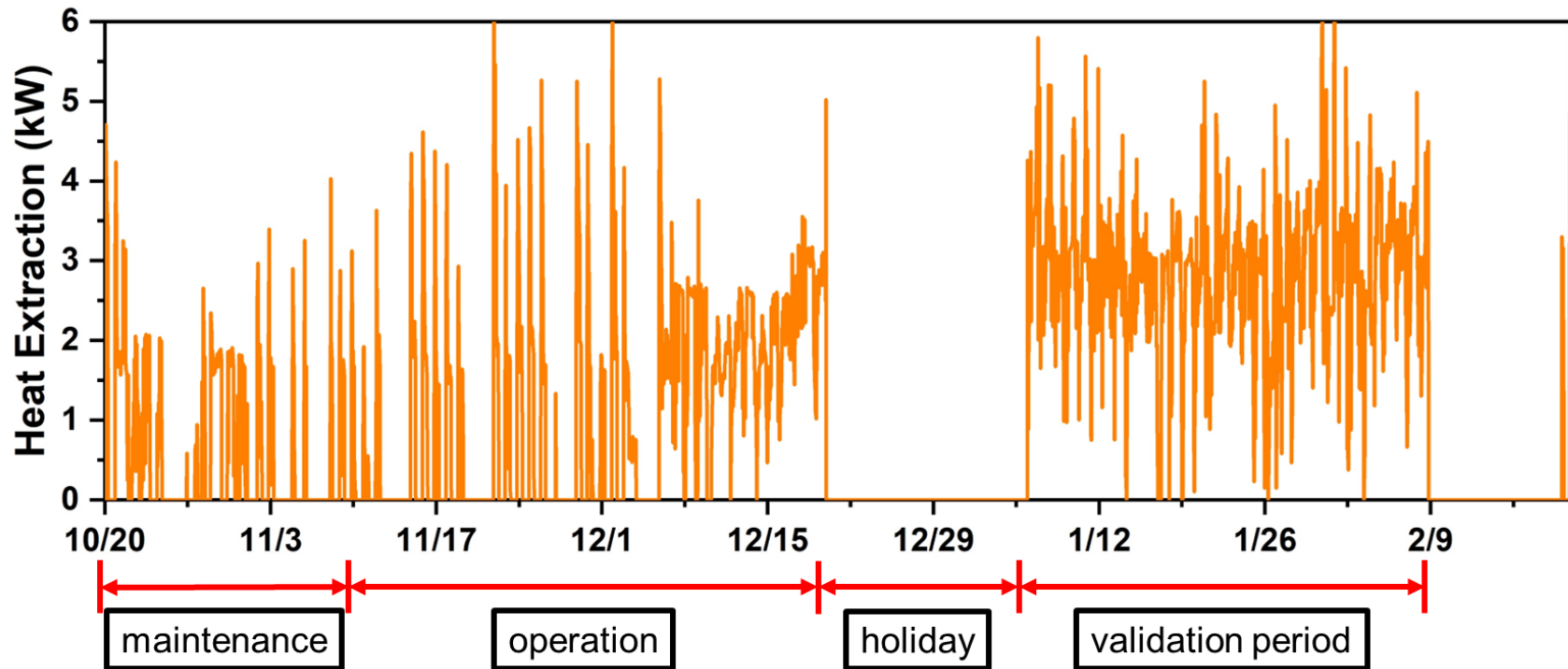
- Root Mean Squared Error (RMSE): **0.73**

- Average temperature:
simulation: 19.71 °C
measurement: 19.77 °C

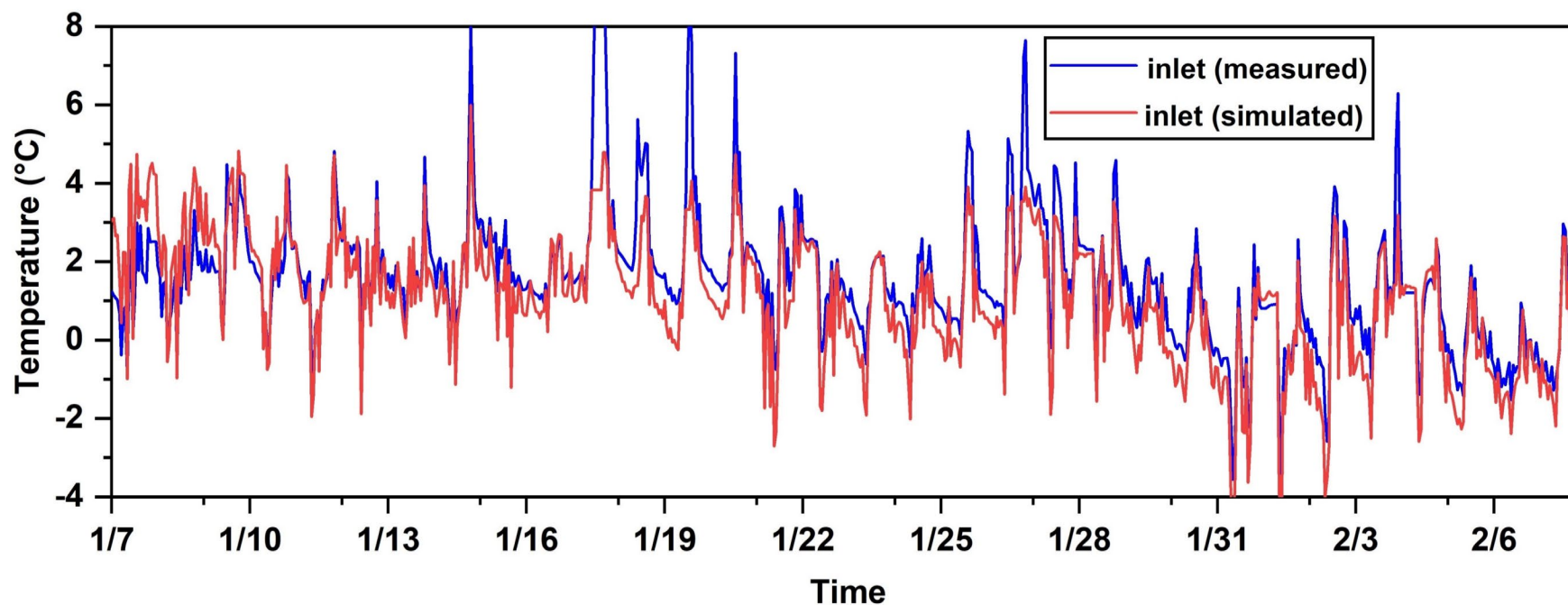
- Small differences when quick temperature changes occur



Space heating operation (winter)



Space heating operation (winter)

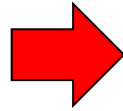


Initial ground temperature: 12 °C

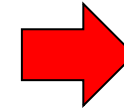
For pipe inlet temperature

- **RMSE: 1.06**
- Average temperature :
simulation: 1.55 °C
measurement: 1.05 °C
- This simulation tool is suitable for GSHP systems using energy pile and spiral GHE.

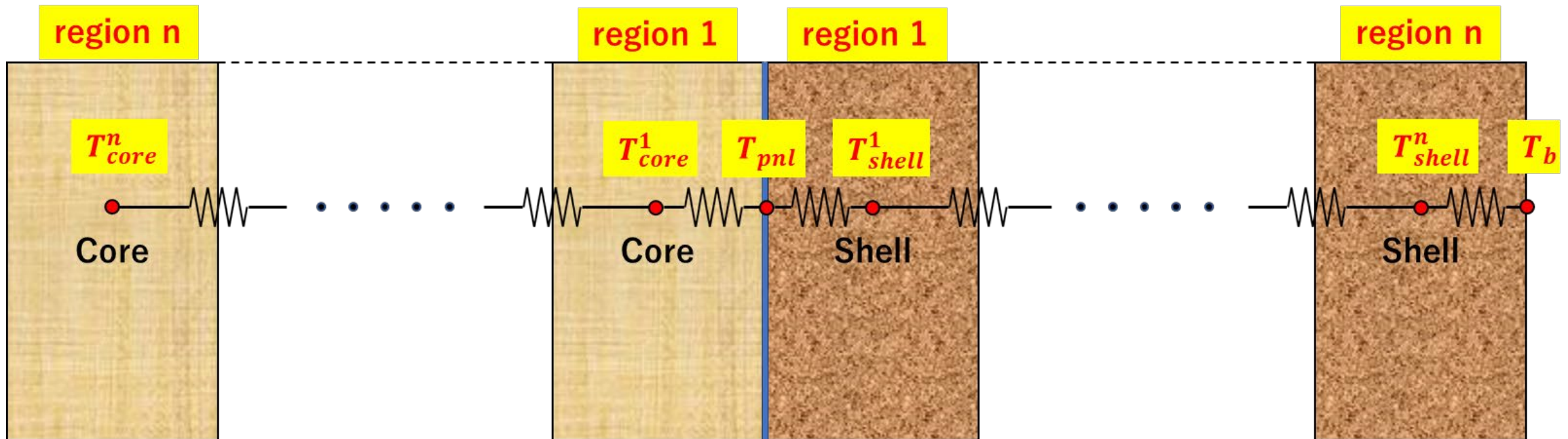
Instantaneous large heat injection

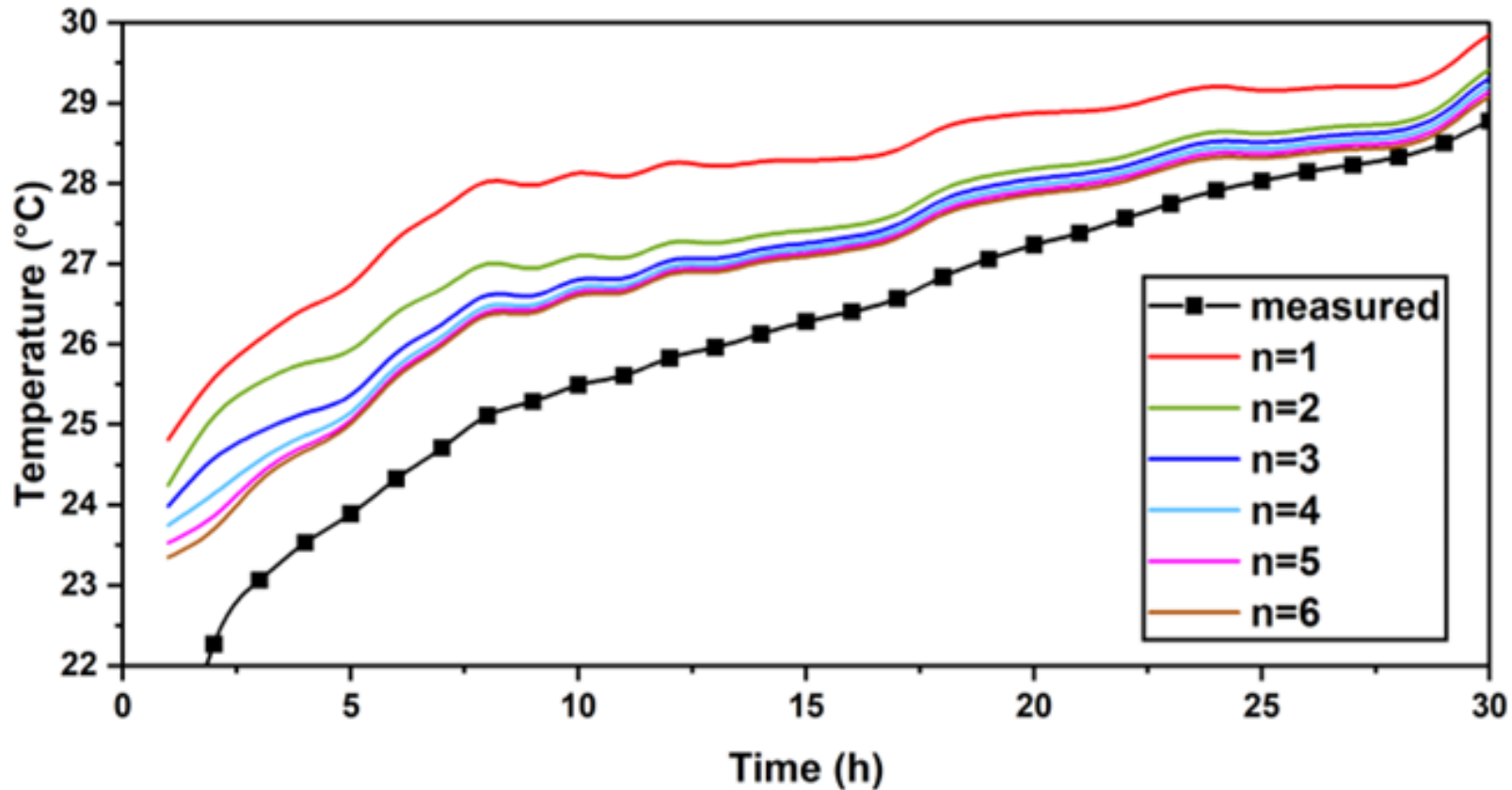


Temperature difference between simulation and measurement



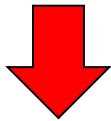
Set up more temperature nodes and divided the core part and shell part into n regions





First 30 hours of TRT

More temperature nodes can make CaRM model be more applicable



The simulation over a short period of time get closer to the actual measurement



Conclusion



1. Using **energy pile** and **spiral GHE** can largely reduce the required land for installation and drilling cost
2. New simulation tool adopting the concept of **fin efficiency** can make the calculation to be simple, fast and accurate
3. This simulation tool is suitable to predict the long-term operation of GSHP systems using energy pile and spiral GHE
4. For short-term operation, setting more temperature nodes can get better simulation results



Thank you for listening