

Optimization of a Residential Air Source Heat Pump using Refrigerants with GWP <150 for Improved Performance and Reduced Emission

Zhenning Li*, Samuel F. Yana Motta, Bo Shen, Hanlong Wan
Oak Ridge National Laboratory, Oak Ridge, TN, USA

Disclaimer:

This manuscript has been authored by UT-Battelle, LLC under Contract No. DE-AC05-00OR22725 with the U.S. Department of Energy. The United States Government retains and the publisher, by accepting the article for publication, acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this manuscript, or allow others to do so, for United States Government purposes. The Department of Energy will provide public access to these results of federally sponsored research in accordance with the DOE Public Access Plan (<http://energy.gov/downloads/doe-public-access-plan>).

- Background
- Objective
- Baseline Heat Pump System & Refrigerants
- Low-GWP Heat Pump Design Optimization Method
- Optimization Results
- Life Cycle Climate Performance Analysis
- Conclusions



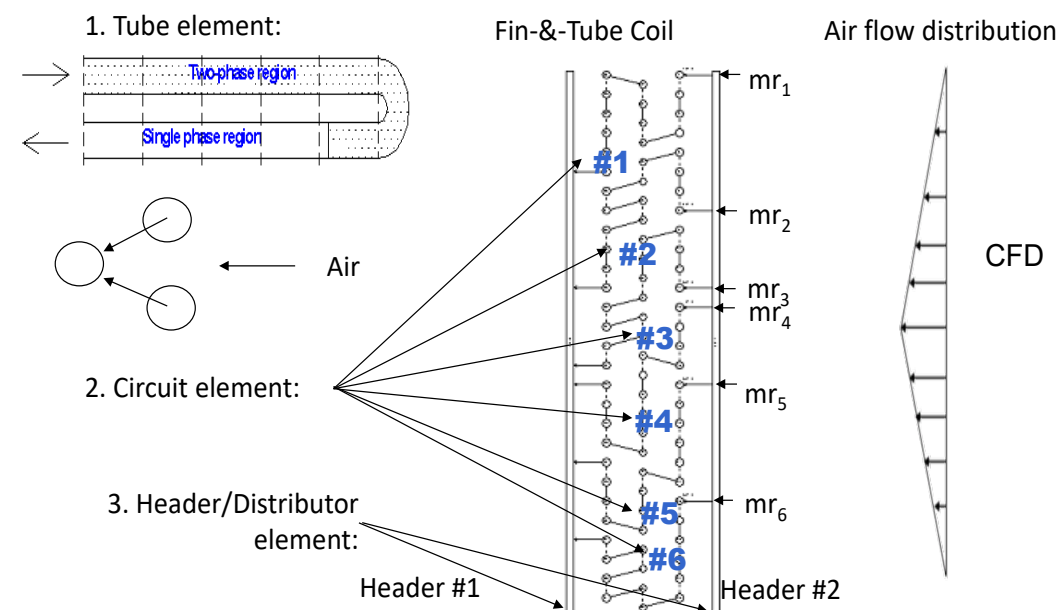
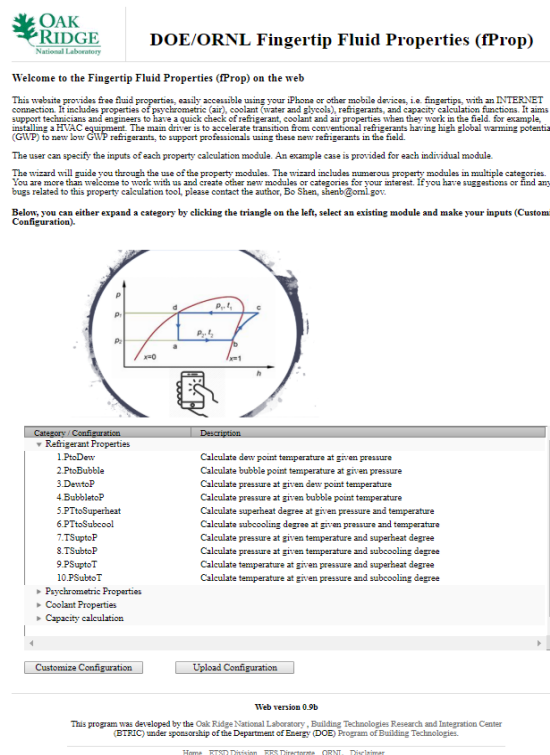
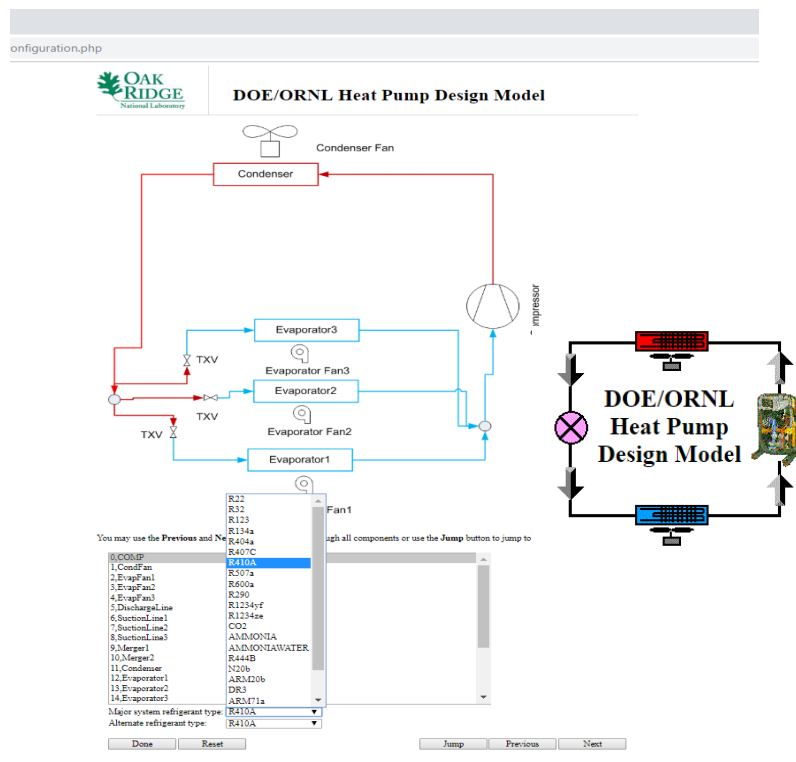
Background



- Environmental concerns are driving a transition in refrigerants
- Many low GWP refrigerants exhibit large temperature glide
 - Requires optimized heat exchanger design for maximum system performance
 - New flow control devices are needed to guarantee heat pump performance under cooling and heating modes
- Most low-GWP mixtures are flammable
 - Heat pump designs must reduce refrigerant charge to reduce risk
- New low-GWP heat pumps must accommodate the current manufacturing and installation processes, and fit into existing homes
- New low-GWP heat pumps must be cost effective and readily accepted by end users

- Evaluate several refrigerant options for residential heat pumps using a modeling tool
 - Consider various refrigerant alternatives
 - Baseline: R410A
 - Short term alternatives with GWP <750: R32, R454B
 - Long-term alternatives with GWP <150: R454C, R455A, R457A, R1234yf, R1234ze(E)
 - Optimize heat exchanger design
 - Maximize energy performance
 - Minimize heat exchanger cost
 - Perform Life Cycle Climate Performance (LCCP) analysis
 - Determine life-time carbon emissions

- Public-domain heat pump design and optimization tool capable of simulating HVAC components and systems using HFC, HFO, natural refrigerants and low-GWP mixtures
- Discretized coil model reveals temperature glide and variation of local properties enabling optimizing coil circuitry

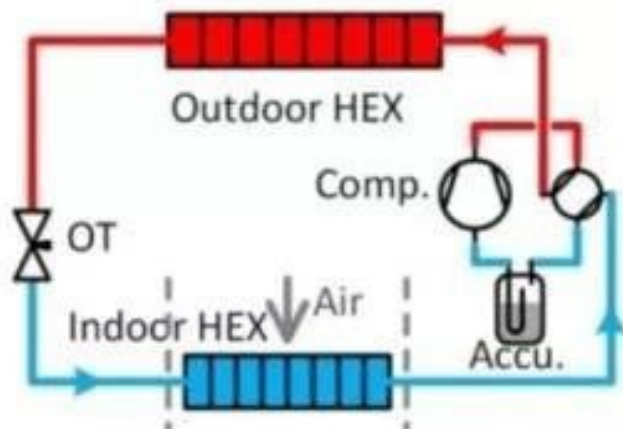


2-D air side distribution; Independent circuit refrigerant entering conditions; Arbitrary circuitry, provides more accurate real-world heat exchanger performance predictions

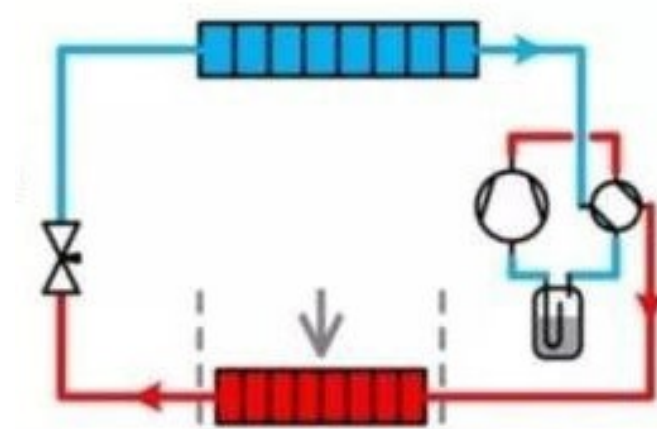


Baseline Heat Pump System

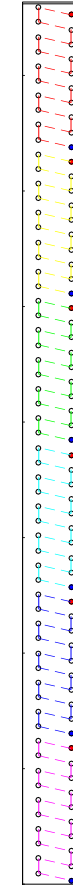
- Refrigerant: R410A
- Nominal cooling capacity: 3 tons
- Single-stage compressor
- Baseline coils: indoor 7 mm-tube, outdoor 9-mm-tube



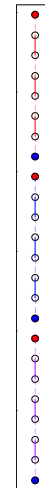
Cooling Mode



Heating Mode



Ø7.95 mm Baseline
Indoor HX
 Mixed flow
 6 Circuits
 120 Tubes
 2 Bank
 60 Tubes per Bank
 Coil height=1.25 m
 Coil length=0.43 m



Ø9.52 mm Baseline
Outdoor HX
 Mixed flow
 8 Circuits
 24 Tubes
 1 Bank
 24 Tubes per Bank
 Coil height= 0.61 m
 Coil length= 2.49 m

Maximize: EER

Subject to:

Operation constraints

$$\Delta T_{\text{superheat, evaporator outlet}} = 10 - \frac{\Delta T_{\text{glide}}}{2} \text{ [R]}$$

$$2 \text{ [R]} \leq \Delta T_{\text{subcooling, condenser outlet}} \leq 15 \text{ [R]}$$

$$Q_{\text{evaporator}} = 10.55 \text{ kW}$$

$$| \text{SHR}_{\text{evaporator}} - \text{SHR}_{\text{baseline, evaporator}} | \leq 1\%$$

$$1 \leq N_{\text{circuits, evaporator}} \leq N_{\text{tubes per bank of evaporator}}$$

$$1 \leq N_{\text{circuits, condenser}} \leq N_{\text{tubes per bank of condenser}}$$

Dimension constraints

$$\text{Height}_{\text{evaporator}} = \text{Height}_{\text{baseline}}$$

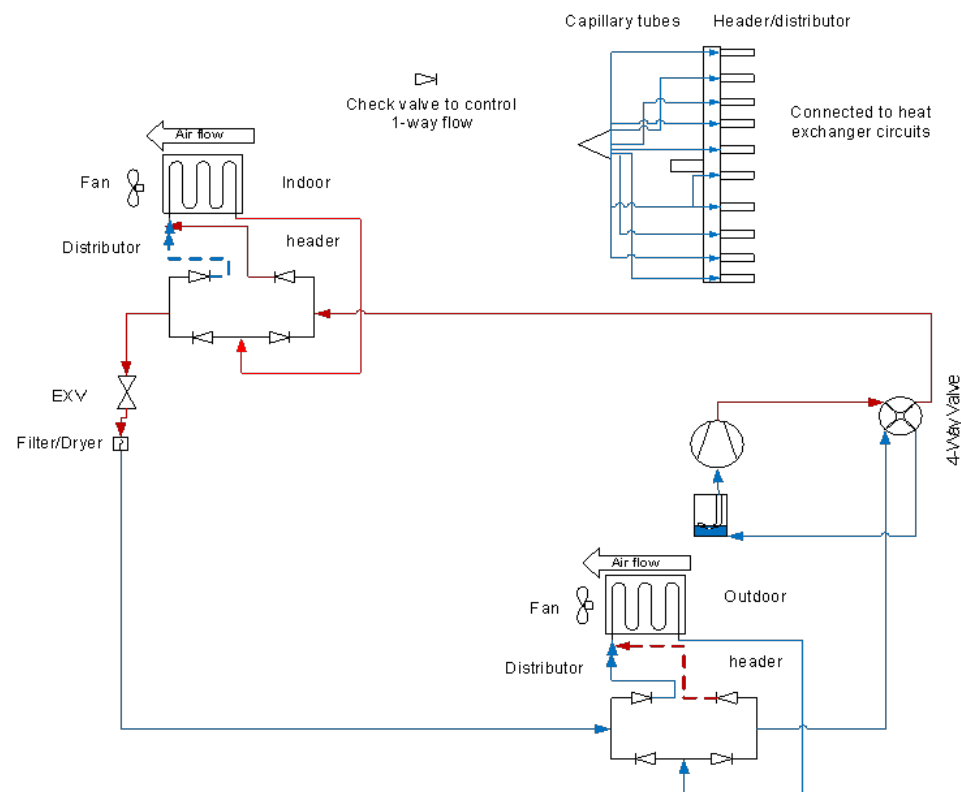
$$\text{Length}_{\text{evaporator}} = \text{Length}_{\text{baseline}}$$

$$\text{Height}_{\text{condenser}} = \text{Height}_{\text{baseline}}$$

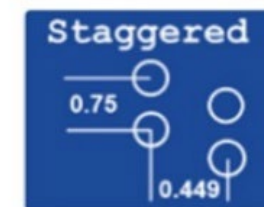
$$\text{Length}_{\text{condenser}} = \text{Length}_{\text{baseline}}$$

Tube diameter varies among 5 mm, 7 mm, 9 mm

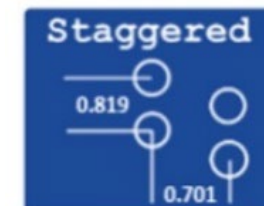
Check-valve assembly to facilitate counter-flow heat exchangers in both cooling and heating modes (arrows in heating mode)



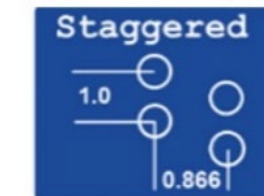
(a) 5-mm Tube Layout



(b) 7-mm Tube Layout



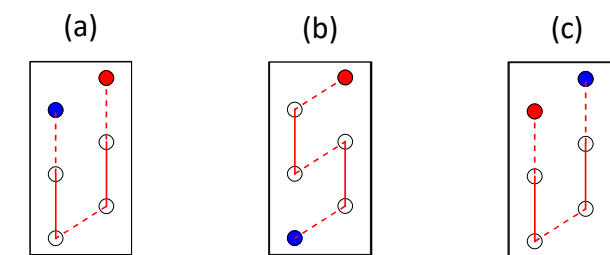
(c) 9-mm Tube Layout



Off-the-shelf tube layout

New System Configuration Maintaining Counter-flow HXs in Dual Modes

Refrigerant	GWP	Safety Class	Composition: Mass Fraction	Glide in Evaporator [K]	Critical Temperature [°C]
R410A	2088	A1	R32/R125: 50%/50%	0.1	72.8
R32	675	A2L	R32: 100%	0	78.1
R454B	466	A2L	R32/R1234yf: 68.9% /31.3%	1.3	78.1
R454C	146	A2L	R32/R1234yf: 21.5% /78.5%	7.7	85.7
R457A	139	A2L	R32/R1234yf/R152a: 18%/70%/12%	6.9	90.1
R455A	145	A2L	R32/R1234yf/CO2: 21.5%/75.5%/3%	11.71	85.61
R1234yf	4	A2L	R1234yf: 100%	0	94.7
R1234ze(E)	4	A2L	R1234ze(E): 100%	0	153.7

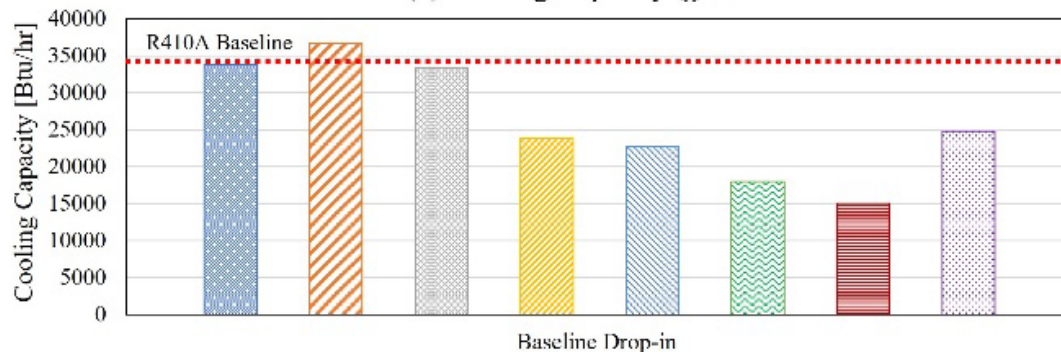


Heat exchanger circuitry patterns
(a) counterflow (b) mixed flow (c) parallel flow

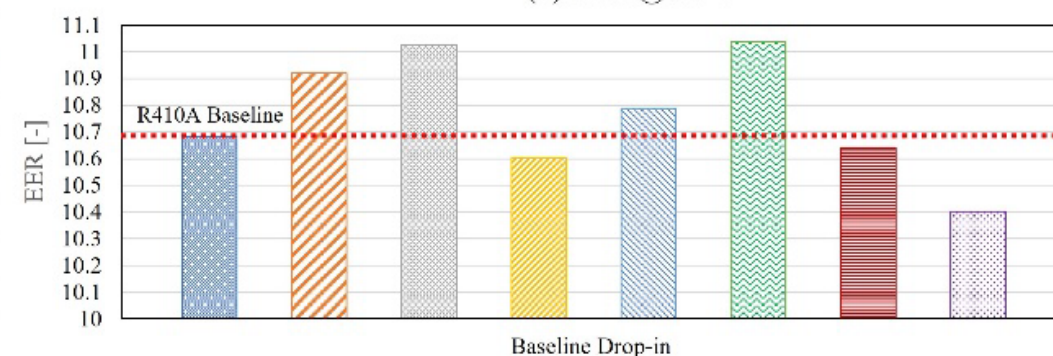
Drop-in Performances for Baseline System

Cooling mode

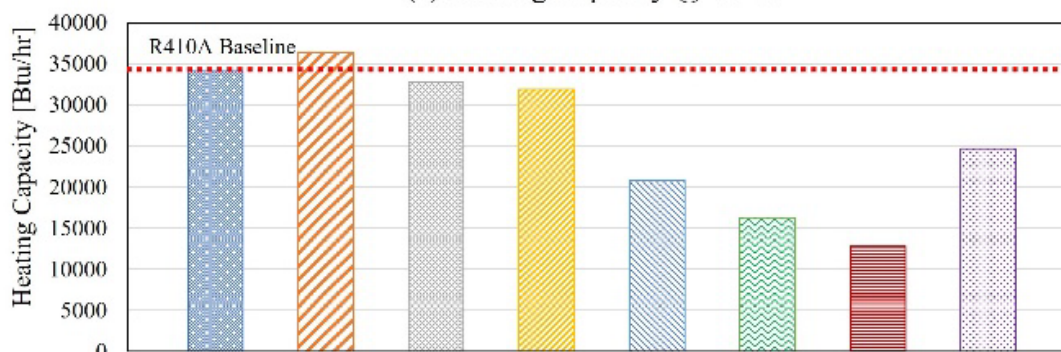
(a) Cooling Capacity @ 95 °F



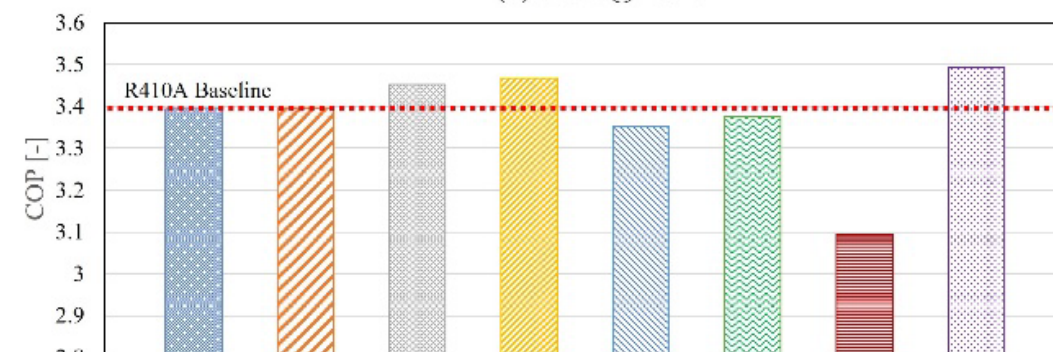
(b) EER @ 95 °F



(a) Heating Capacity @ 47 °F

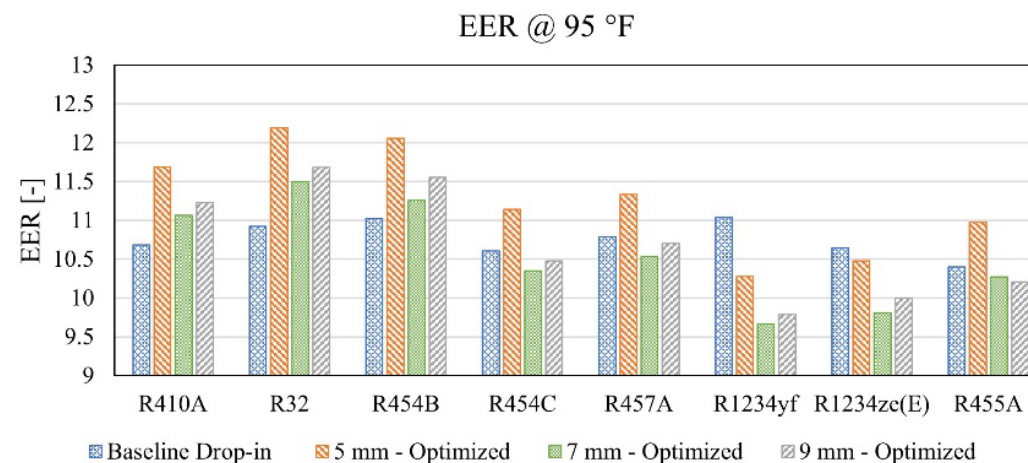


(b) COP @ 47 °F

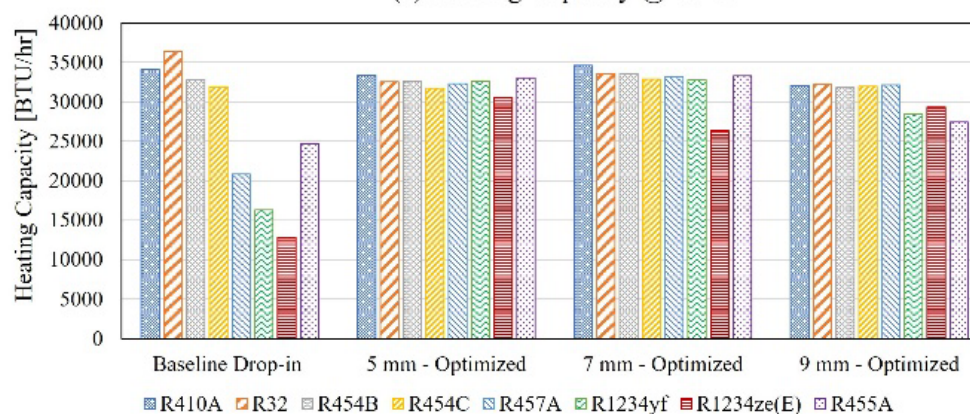


Heating mode

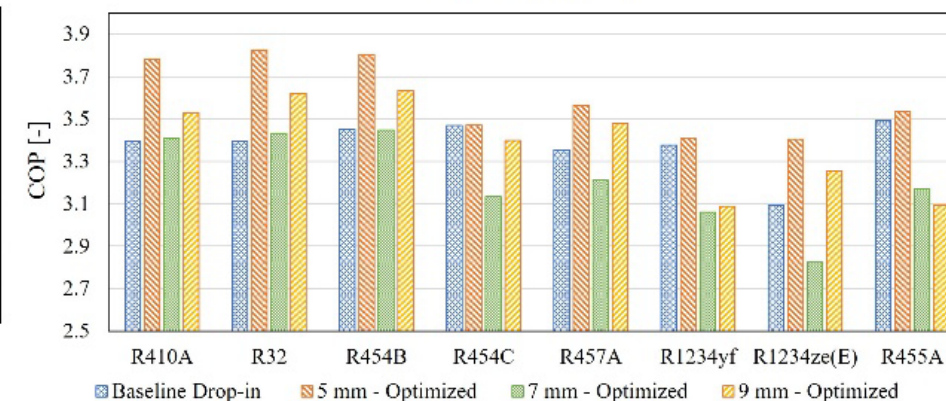
Cooling mode



(a) Heating Capacity @ 47 °F



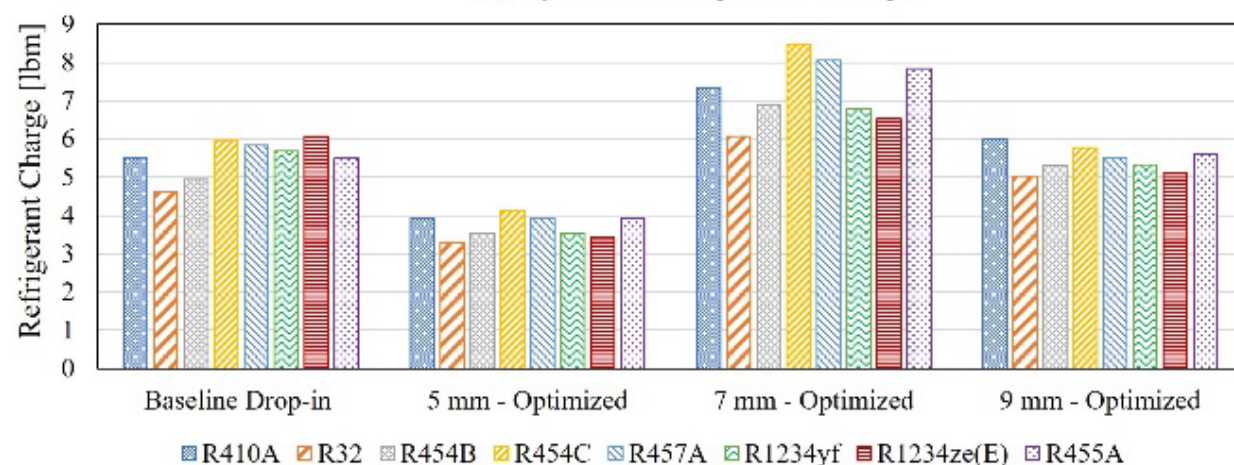
(b) COP @ 47 °F



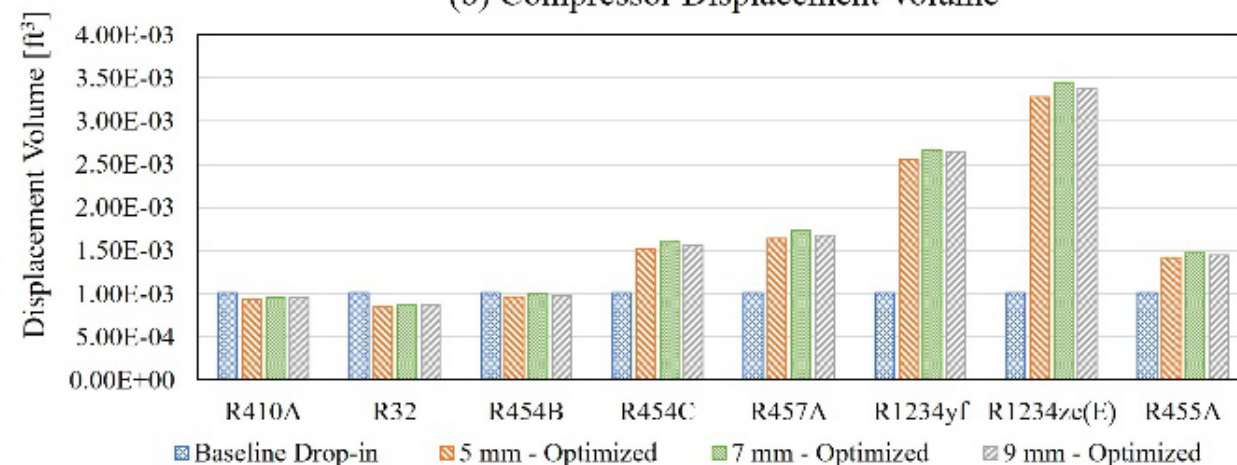
Heating mode

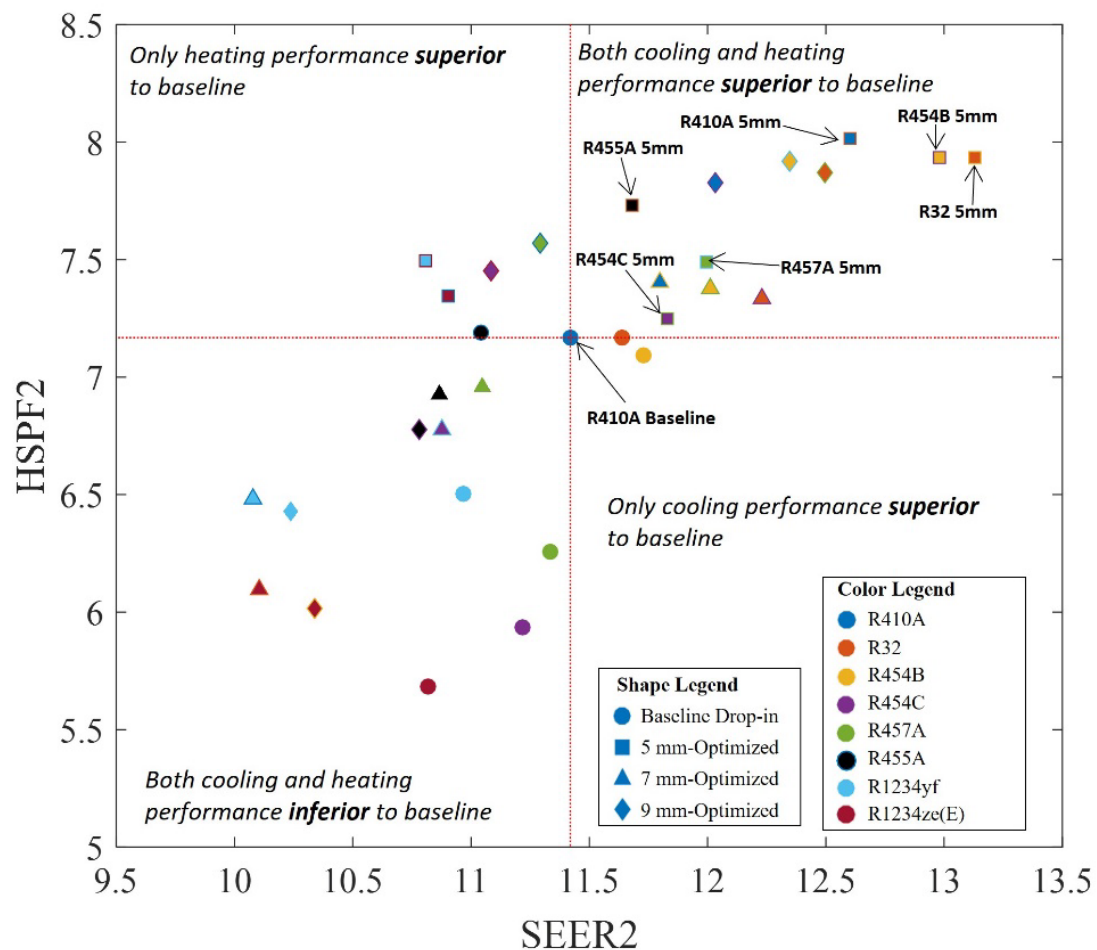
- Compressor displacement volume is optimized for each low-GWP refrigerant at AHRI 210/240 Test Condition A to target the same cooling capacity
- The compressor isentropic efficiency is fixed as 0.74 and the volumetric efficiency is fixed at 0.98 to be consistent with the baseline R410A system

(a) System Refrigerant Charge



(b) Compressor Displacement Volume





Heat Exchanger Structure of Optimized Systems*

HX Structure	5 mm - Optimized		7 mm - Optimized		9 mm - Optimized	
	Indoor HX	Outdoor HX	Indoor HX	Outdoor HX	Indoor HX	Outdoor HX
R410A	64x3-16	32x2-16	60x2-6	30x2-6	48x2-6	24x1-2
R32	64x3-16	32x2-16	60x2-6	30x2-5	48x2-6	24x1-2
R454B	64x3-16	32x2-16	60x2-6	30x2-10	48x2-4	24x1-2
R454C	64x3-32	32x2-16	60x2-12	30x2-6	48x2-6	24x1-3
R457A	64x3-32	32x2-16	60x2-12	30x2-6	48x2-6	24x1-3
R455A	64x3-32	32x2-16	60x2-15	30x2-6	48x2-8	24x1-3
R1234yf	64x3-32	32x2-16	60x2-15	30x2-6	48x2-8	24x1-3
R1234ze(E)	64x3-32	32x2-16	60x2-15	30x2-6	48x2-8	24x1-3

*HX Structure Naming Convention: "Number of Tubes per Row x Number of Rows - Number of circuits"

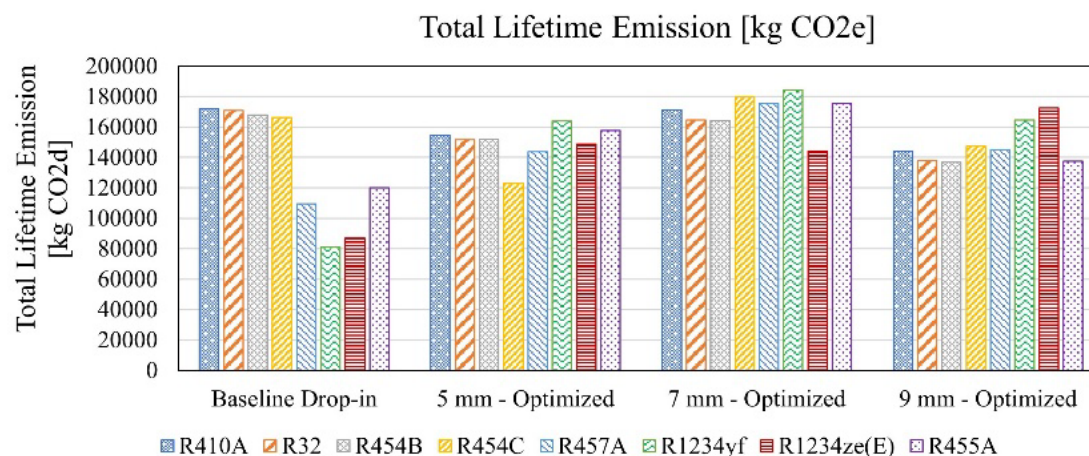


Life Cycle Climate Performance (LCCP) Analysis

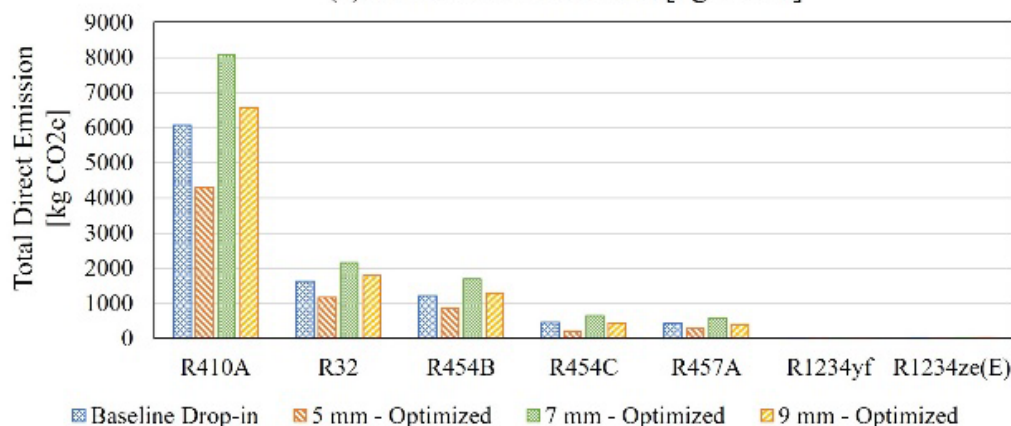


- Determine life-time carbon emissions of the HP designs
 - *Direct emissions:* Refrigerant release during operation and at End-of-Life (EOL)
 - *Indirect emissions:* From energy consumption, manufacturing of materials and unit, manufacturing of refrigerants and disposal of unit

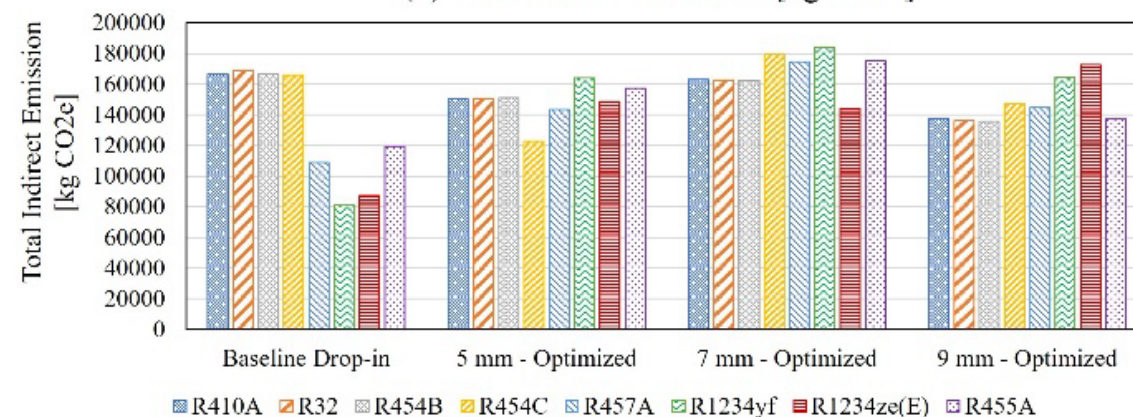
Factor	Value
Refrigerant	R410A or its alternatives
Refrigerant charge (kg)	Obtained from System Simulation
Unit weight (kg)	190
Annual refrigerant leakage (%)	2
EOL leakage (%)	80
Lifetime (years)	18
Cut-off temperature (°C)	-17.8
Temperature at which the heat pump starts (°C)	-12.2
Weather data	Chicago TMY-3



(a) Total Direct Emission [kg CO₂e]



(b) Total Indirect Emissions [kg CO₂e]



- To support the transition to refrigerants with $GWP < 150$ and high glide
 - New heat exchanger designs
 - New flow control schemes
 - New compressors
- Improved performance possible, with reduced refrigerant charge and reduced lifetime carbon emissions
- Higher efficiencies in both cooling and heating modes than R410A baseline system are achieved using refrigerants with $GWP < 150$
- Establish a production and installation path to produce cost-effective low-GWP heat pumps which will be readily accepted by end users



Thank you!

Zhenning Li

Building Equipment Research Group

Oak Ridge National Laboratory

Email: liz5@ornl.gov

Phone: 301.503.8568