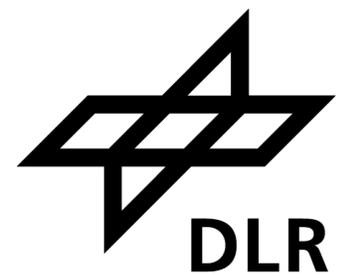


# Numerical evaluation of high-temperature heat pump and thermal energy storage system for industrial processes

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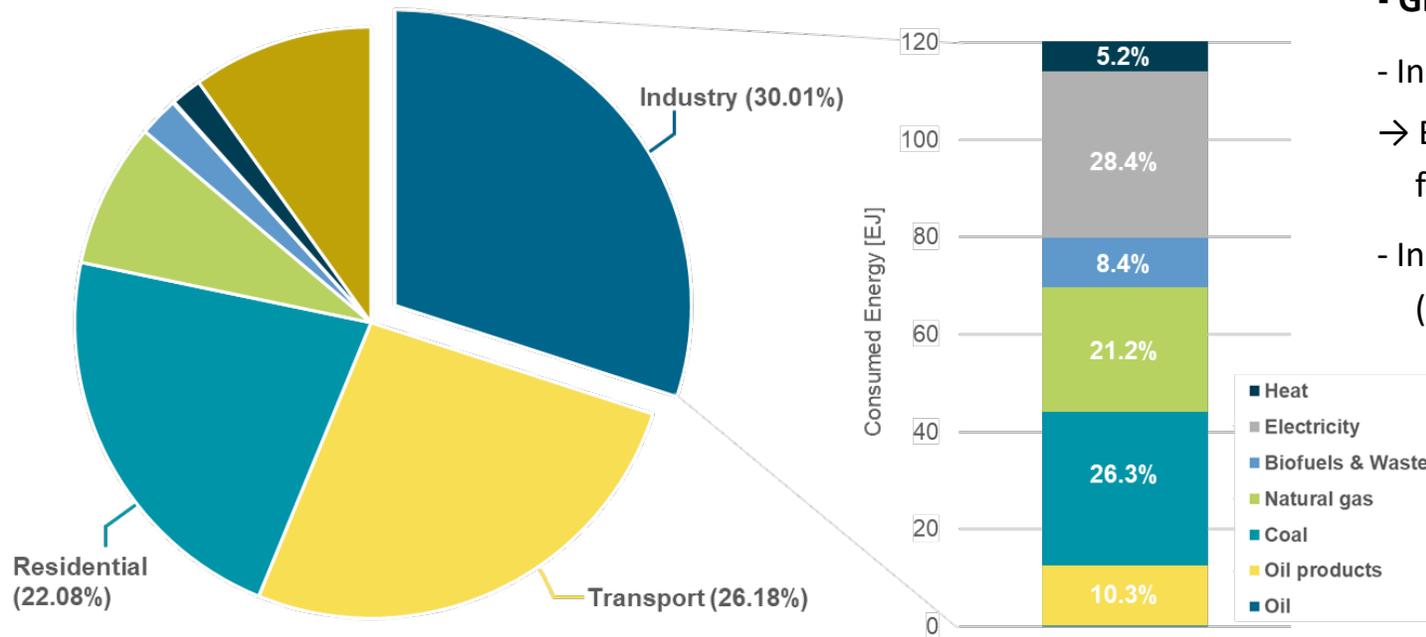
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- **Background  
(Heating demands in industrial)**
- **Modeling of HTHP  
& TES systems**
- **Results & Analysis**
- **Conclusions**

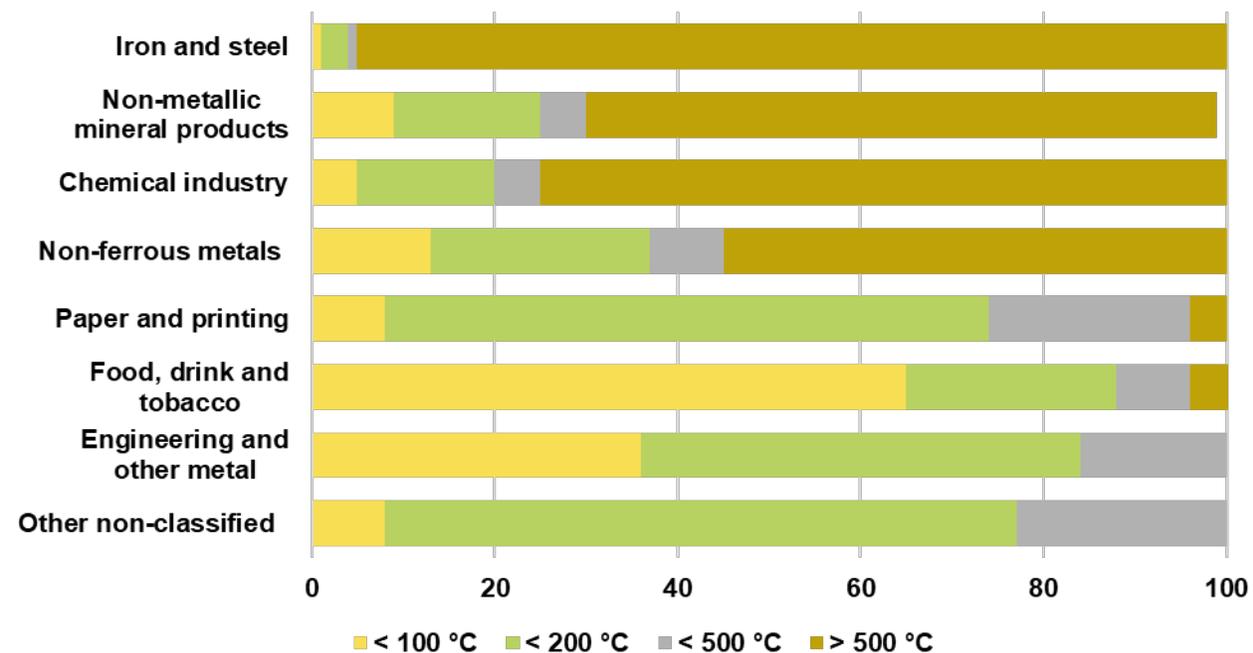




- **Global industrial energy consumption & greenhouse emission**
- Industrial process is the world's largest final energy consumer (120 EJ).
- By considering electricity generated from fossil fuel, > 75% of energy used for industrial processes (> 90 EJ) comes from fossil fuels.
- Industrial processes emit 24% of the global greenhouse gas in 2019 (14 GtCO<sub>2</sub>eq) with the exception of energy sector.

**Electrification can be an effective option for reducing greenhouse gas emissions from the industry.**

**Fig.** Total Energy consumption by sector & Energy carrier for industrial sector, World 2022 [IEA].



## Temperature levels by industrial subsectors

- Consumed temperature levels correlate with specific subsectors.
- < 100°C: F&B, 100-500°C: Pulp & Printing, > 500°C: Iron & Steel.
- Process heat supplying methods and systems can be divided into 500°C.
- < 500°C: Steam & Hot water, > 500°C: Industrial furnace.

## High-Temperature Heat Pump (HTHP) for industrial processes

- HTHP has high potential to efficiently recover waste heat from industrial process and upgrade it to higher temperature.
- If zero-carbon electricity is used in the processes, the GHG emissions of the industrial site can be significantly reduced.

Fig. Temperature distribution by subsector [EU Commission 2016 (WP1)].

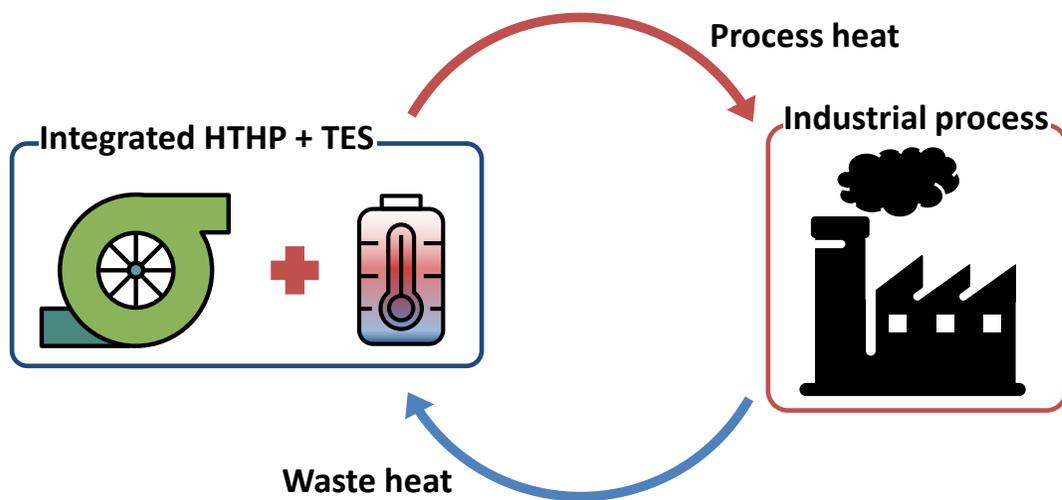


Fig. Image of working principle about HTHP + TES system.

## ▪ Thermal Energy Storage (TES) system

- TES systems are mainly used to overcome the mismatch between energy generation and demand (Temp., Location, or Power difference).  
→ Sensible heat storage, Latent heat storage, Thermochemical storage.
- TES technology can improve the efficiency of heat pumps.

## Object of this study

Performance Evaluation and Comparison of HTHP and Two Different TES Integrated Systems (SHS and TCES)

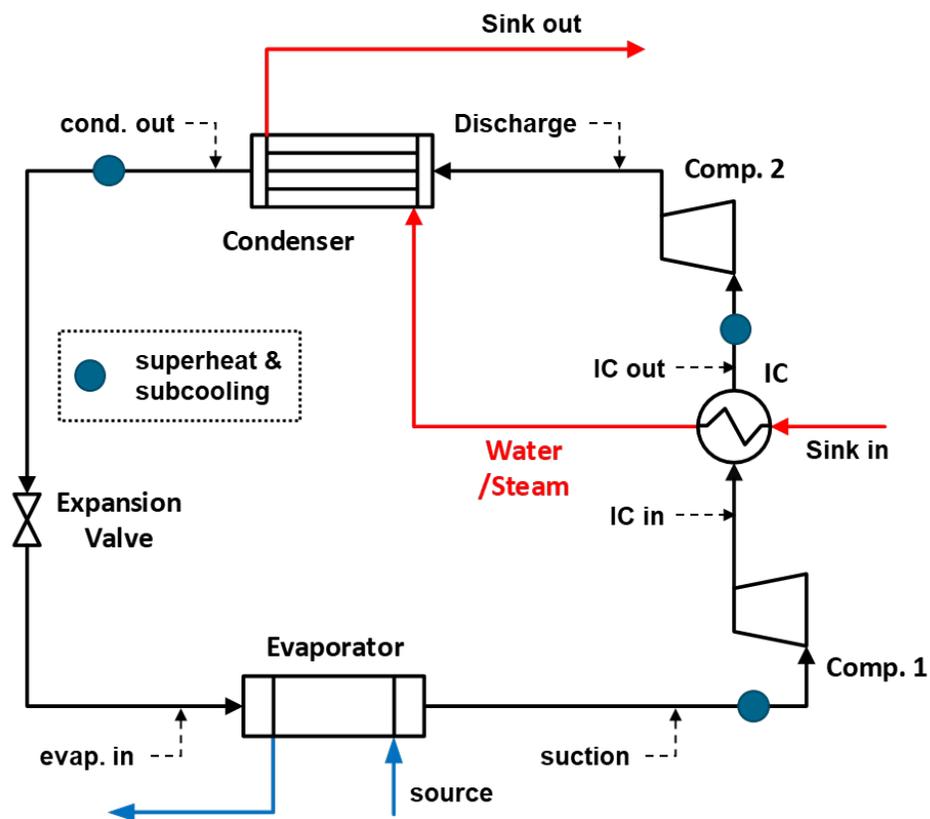


Fig. Schematic diagram of main HTHP cycle.

## Modelling & Boundary conditions

- Two-stage water vapor compression cycle with intercooling.
- Both compressors have same pressure ratio.
- Boundary and operating conditions.

HTHP	Values	TES	Values
$T_{\text{evap}}/T_{\text{cond}}$	90°C/160°C ( $\Delta T = 70 \text{ K}$ )	$\dot{Q}_{\text{sink}}$	$\dot{Q}_{\text{stor.}} = 500 \text{ kW}$
$\eta_{\text{iso}}/\eta_{\text{mech}}$	0.78/0.95	$\tau_{\text{stor}}$	8 hrs (28800 s)
$T_{\text{source/sink in/sink out}}$	110°C/25°C/200°C	$P_{\text{sink}}$	$P_{\text{sink}} = P_{\text{cond}}$
$T_{\text{sup \& sub}}$	10 K	$m_{\text{sink}}$	$m_{\text{sink}} = m_{\text{stor \& dis}}$

- Parameters of entire HTHP are determined based on Enthalpy/Entropy balance.
- $W_{\text{comp}}$ : 113.4 kW and COP: 4.4.

\*Properties for Water/Steam: IAPWS-IF97.

## ▪ Modeling of Sensible Heat Storage system

- Concrete was considered as a SHS material.

→ Properties for 200°C are used ( $C_p$ ,  $\rho$ , and so on).

## ▪ Charge/Discharge operations

- Charge:  $T_{char.}$  is 190°C and the required amounts of concrete is obtained.

- Discharge:  $T_{dis.}$  can be controlled by regulating the  $\dot{m}_{air-dis.}$

→ Due to  $P_{sink} = P_{cond}$ , phase shift in water/Steam depending on  $T_{cycle out}$

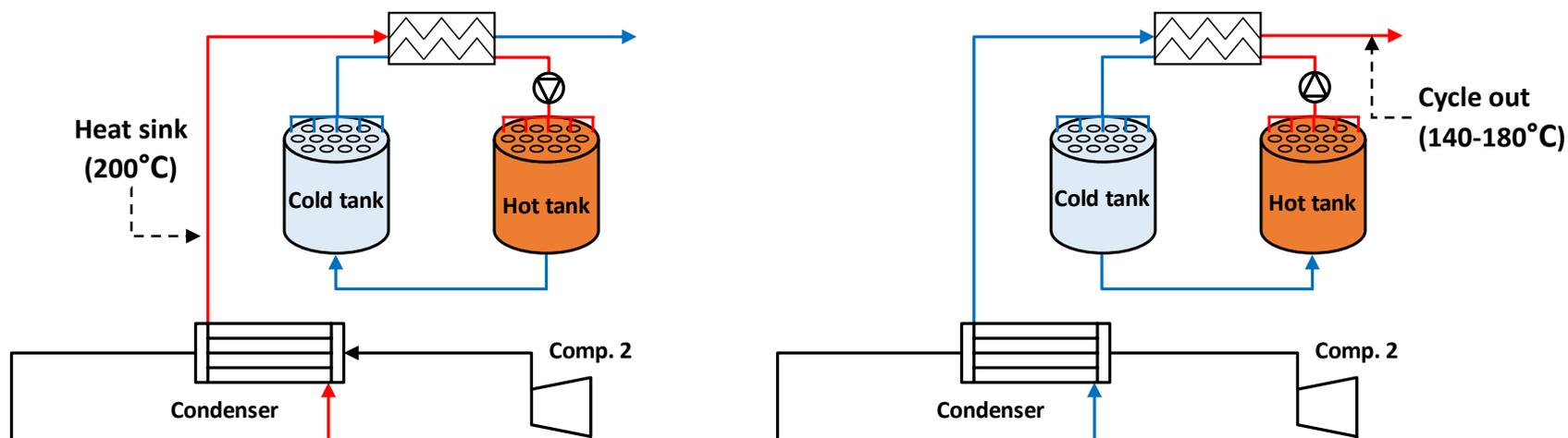


Fig. Image of pumped thermal energy storage: (left) Charge, (right) Discharge mode.

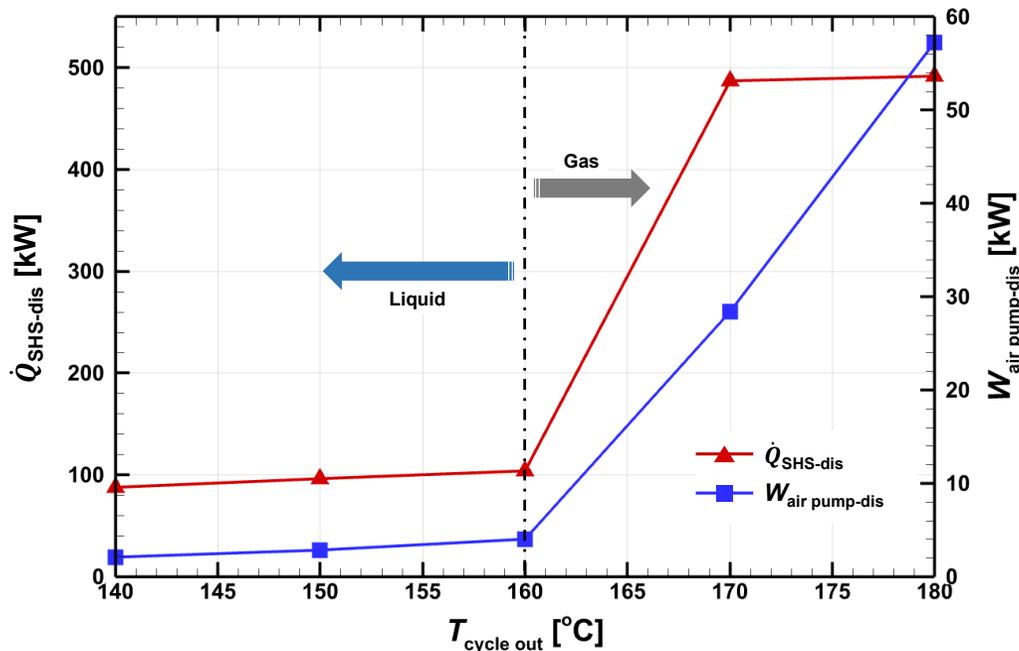


Fig. Changing of  $Q_{\text{SHS-dis}}$  and  $W_{\text{air pump-dis}}$ .

## ▪ Specification of SHS system

- Required amount of concrete for SHS system.

→  $m_{\text{concrete}} = 96,647 \text{ kg}$ ,  $V_{\text{concrete}} = 43.0 \text{ m}^3$ .

- Corresponded  $\dot{m}_{\text{air}}$  and  $W_{\text{air pump}}$  are changed for each operation.

→ Charge:  $\dot{m}_{\text{air}} = 2.82 \text{ kg}$ ,  $W_{\text{air pump}} = 3.5 \text{ kW}$ .

→ Discharge:  $\dot{m}_{\text{air}} = 1.66\text{-}45.89 \text{ kg}$ ,  $W_{\text{air pump}} = 2.1\text{-}57.3 \text{ kW}$ .

## ▪ Modeling of Thermochemical Energy Storage system

- Strontium bromide and Water system ( $\text{SrBr}_2/\text{H}_2\text{O}$ ).

→  $\text{SrBr}_2 (\text{s}) + \text{H}_2\text{O} (\text{g}) \leftrightarrow \text{SrBr}_2 \cdot \text{H}_2\text{O} (\text{s})$ ,  $\Delta H_{\text{SrBr}_2} = 71.98 \text{ kJ/mole}$ .

→  $\text{H}_2\text{O} (\text{g}) \leftrightarrow \text{H}_2\text{O} (\text{l})$ ,  $\Delta H_{\text{H}_2\text{O}} = 40.65 \text{ kJ/mole}$ .

- Packed bed reactor system is adopted.

## ▪ Charge/Discharge operations

- Charge:  $\text{SrBr}_2 \cdot \text{H}_2\text{O}$  is decomposed at  $190^\circ\text{C}$ .

- Discharge: Waste heat from industrial processes is assumed at  $110^\circ\text{C}$ .

→ Discharge performance has been estimated by using equilibrium pressure.

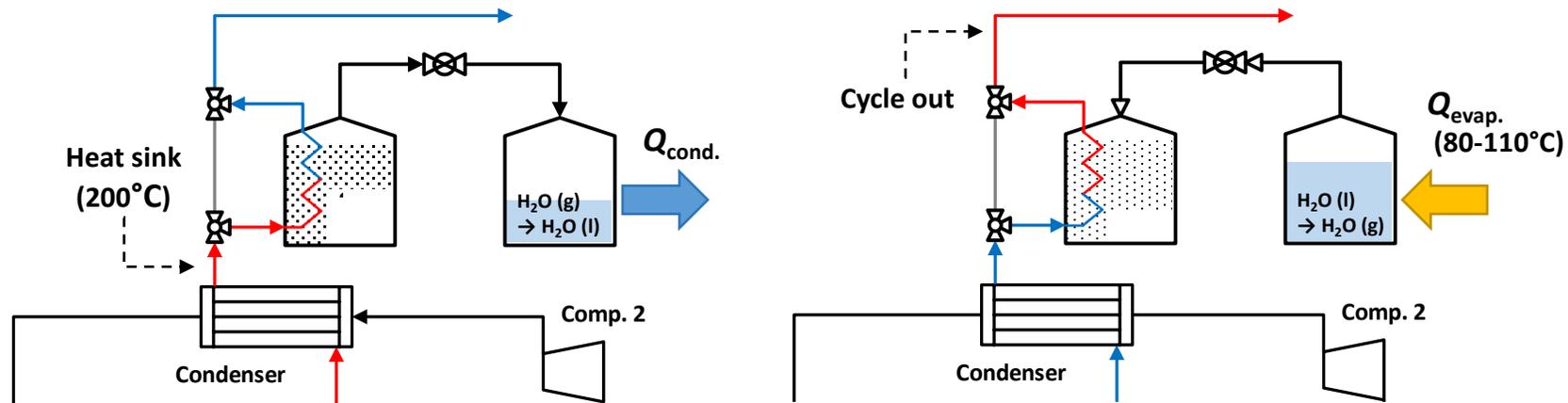


Fig. Image of thermochemical energy storage system: (left) Charge mode, (right) Discharge mode.

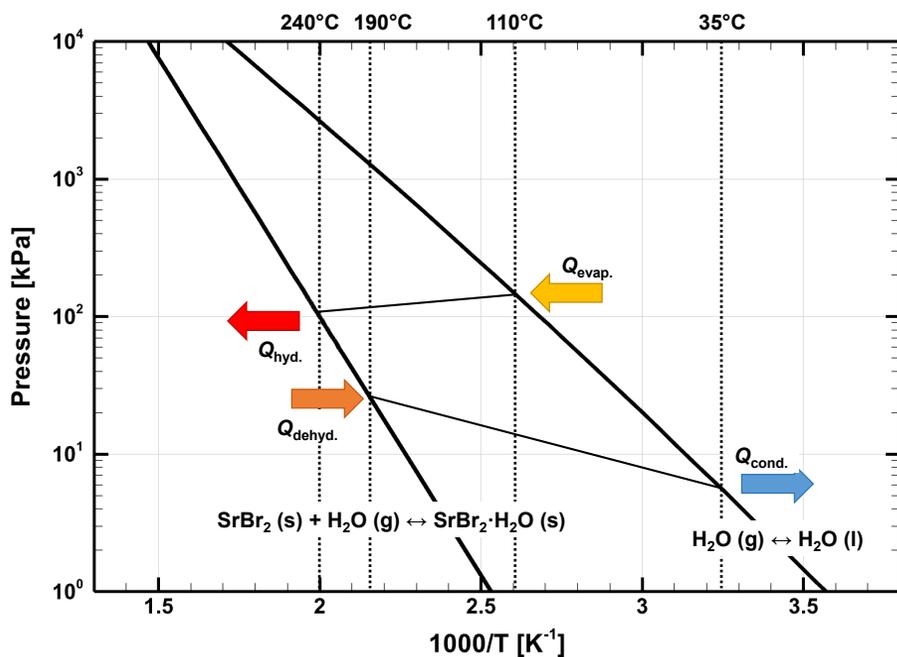


Fig. Van't Hoff diagram of SrBr<sub>2</sub>·H<sub>2</sub>O solid-gas reaction.

- SrBr<sub>2</sub>/H<sub>2</sub>O working pair for TCES system

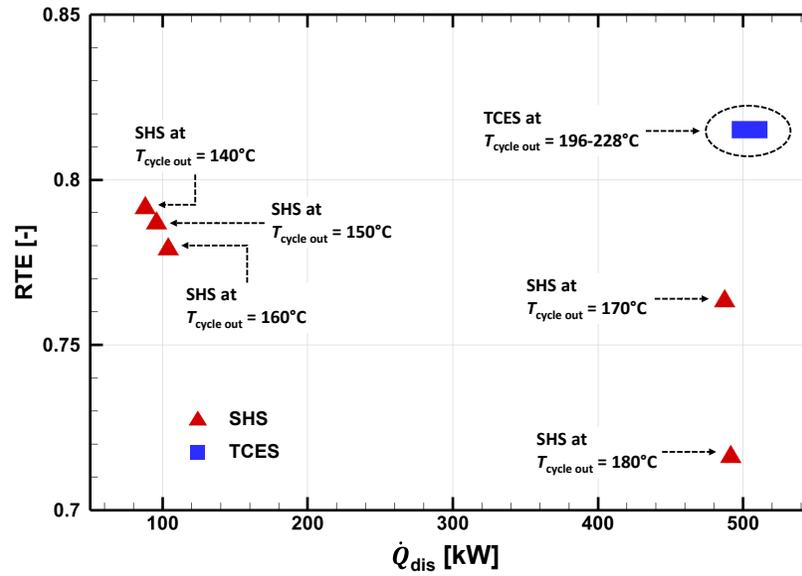
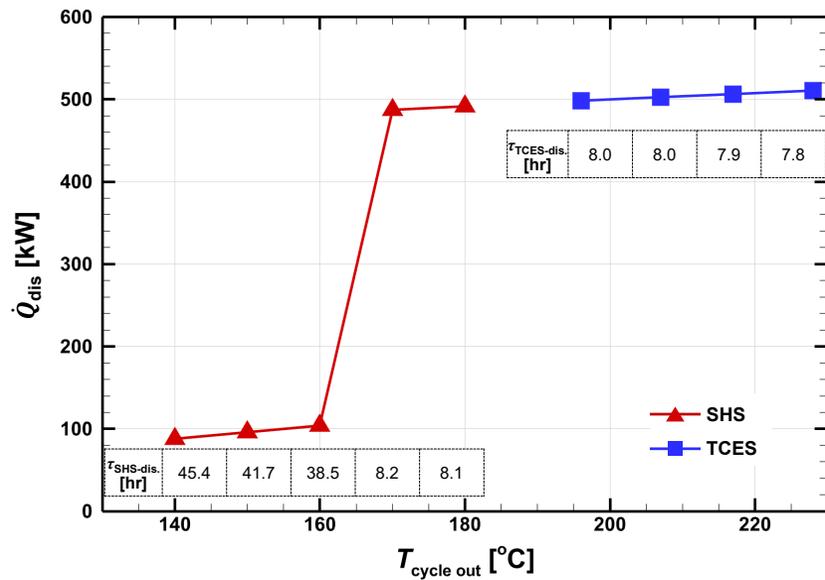
- Van't Hoff equation for a reversible solid-gas reaction (SrBr<sub>2</sub>·H<sub>2</sub>O).

$$\ln K_{eq}(T, P) = \ln \left( \frac{P}{P^0} \right) = \frac{\Delta G}{RT} = -\frac{\Delta H}{RT} + \frac{\Delta S}{R}$$

- Water-vapor saturation table is used for water/steam line.

- Discharge performance of TCES system

$T_{evap.}$ [°C]	$T_{hyd.}$ [°C]	$\tau_{dis.}$ [hrs]	$\dot{Q}_{TCES-dis.}$ [kW]
80	206	8.03	498
90	217	7.96	502
100	227	7.90	506
110	238	7.80	510



## Comparison of both TES systems

- TCES has higher  $T_{cycle out}$  and  $\dot{Q}_{dis}$  than SHS.
- Round Trip Efficiency (RTE) of TES systems.
- Air pump power consumption affects RTE difference (SHS: 0.72-0.79, TCES: ~0.82).

$$\eta_{RT} = \frac{(\dot{Q}_{cycle out} - P_{o,pump dis}) \times \tau_{dis}}{(\dot{Q}_{sink} + W_{comp.} + P_{o,pump char}) \times \tau_{stor.}}$$

Fig. Results of comparison: (left)  $\dot{Q}_{dis}$  and  $\tau_{dis}$  in function of the  $T_{cycle out}$ , (right) RTE according to  $\dot{Q}_{dis}$ .

## ▪ Comparison of both TES systems

- TCES system has the advantage of being compact in size.
- High energy density of thermochemical reaction results in compact system.
- TCES system can supply a higher temperature than it was stored.

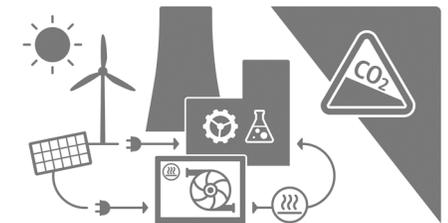
**Table.** Specifications of TES systems.

	SHS	TCES	Note
<b>Material</b>	Concrete	$\text{SrBr}_2 \cdot \text{H}_2\text{O}$ ( $\text{SrBr}_2$ )	TCES/SHS
<b>Weight</b>	96,647	53,101 (49,500)	0.55 (0.51)
<b>Volume</b>	43.0	13.6 (11.7)	0.32 (0.27)

**An effective HTHP + TES system can decarbonize industrial processes**

## ▪ Future works

- Investigating the effects of different temperature conditions.
- Develop the transient simulation model for HTHP-TES system.
- Practical economic analysis of HTHP-TES system.
- Pilot plant test of HTHP-TCES system for industrial application.





**THANK YOU FOR YOUR ATTENTION**