

MEASURED THERMAL PERFORMANCES OF THE DOCK MIDFIELD GROUND SOURCE SYSTEM AT ZÜRICH AIRPORT

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Abstract: The Dock Midfield is the new terminal E of the Zürich airport. A 630 kW heat pump at S4W40 operative conditions is coupled to about 300 piles to contribute to the building heating and cooling. Measurements of the energy pile system begun in October 2004 for a 2 years period. The results of the measurement campaign are presented. The global system efficiency, defined as heating and cooling energy divided by all the electrical energy used to operate the system, lies over 5. Cooling energy is provided by geocooling, i.e. by coupling the cooling distribution to the pile flow loop with a flat plate heat exchanger, and the heat pump used as a cooling machine. Simulations performed with PILESIM2 have shown that cooling energy delivered at 16 – 17°C instead of 14°C would not require the use of the cooling machine. The global system efficiency would increase from 5.1 to 5.7. From an economical point of view, the pile system is more convenient than a conventional system. The additional investment of the pile system is paid back in about 8 years.

Key Words: *heat pump, energy pile, UTES, geocooling, system efficiency*

1 INTRODUCTION

Dock Midfield is the new terminal E of the Zürich airport. Designed for 26 planes, the building (500 m long and 30 m wide) is built on 440 foundation piles as the upper ground layer, which is composed of lake deposits, is too soft to support the loads of the building. The piles stand on moraine, which lies at a depth of about 30 m. With a diameter of 0.9 to 1.5 meters, the concrete piles were cast in place. An image of the building is shown in figure 1.



Figure 1: The Dock Midfield of the Zürich airport has been built on 440 foundation piles of 30m

Renewable energies are used extensively throughout this building. Renewables are expected to meet 65% and 70% of the heating and cooling requirements respectively. The foundation piles contribute by being used as energy piles: about 300 piles have been equipped with 5 U-pipe fixed on the metallic reinforcement to use them as a heat exchanger with the ground. They form an underground thermal energy storage (UTES) for heating and cooling. The additional amount of energy purchased for heating is very small. The associated heating energy index, defined by the ratio of the annual purchased energy (district heating

energy and electricity for the heat pump) per the total heated floor area (85'200 m² with height correction), is about 15 kWh/(m²y). The total electric energy index, estimated to 110 kWh/(m²y), is also low for a fully air conditioned building which is used 18 hours a day.

Construction of the Dock Midfield started in 1999 and was completed in 2003. In September 2004, the measurement of the pile system started for a two years period.

The main objectives of the measurement project, whose purpose concentrates on the pile system, are to:

- determine the system thermal performances;
- check the validity of the design procedures;
- highlight the importance of an integrated approach in the design phase;
- optimize system operation.

The measurements were used to improve the simulation tool PILESIM. The new version, called PILESIM2 (Pahud 2007), better takes into account geocooling calculations in a system. Geocooling is cooling energy from the ground covered without a cooling machine. It is realized by coupling the building cooling distribution directly to the pile hydraulic circuit through a conventional heat exchanger.

2 THE ENERGY PILE SYSTEM

The heat pump coupled to the piles has been sized so that the fluid temperature in the pile circuit never drops below 0°C, both for short term and long term system operation (Pahud and al. 1998, 1999; Documentation SIA D0190 2005). It delivers a heating power of 630 kW at the temperature conditions B4W40. Peak power loads are met with district heating used in complement to the heat pump. 85% of the annual heating demand, which was established to 2'720 MWh/y, should be covered by the heat pump. The cooling requirements are met by a cooling distribution network coupled to the pile system (1'240 MWh/y) and the building ventilation system with conventional cooling machines (510 MWh/a). Cooling energy covered by the pile system is either made by geocooling or for heating purposes, if the heat pump is in operation. The return fluid temperature in the cooling distribution is expected to be 21°C. The forward one is set to 14°C. If geocooling is not sufficient to meet the cooling demand, the heat pump is used as a cooling machine. Its waste heat is dumped in cooling towers placed on the roof of the building. Table 1 contains the main characteristics of the piles.

Table 1: Main characteristics of the energy piles forming the ground heat exchanger of the UTES

Type of foundation pile	cast in place, in concrete
Number of energy piles	306
Pile diameter	90 – 150 cm
Average active length per pile	26.8 m
Number of U-pipes per pile	5 (10 pipes in a pile cross-section)
Ground volume thermally activated by the piles	660'000 m ³
Flow rate per pile	max. 860 litres/h

The system layout of the pile system and the measurement points are shown in figure 2.

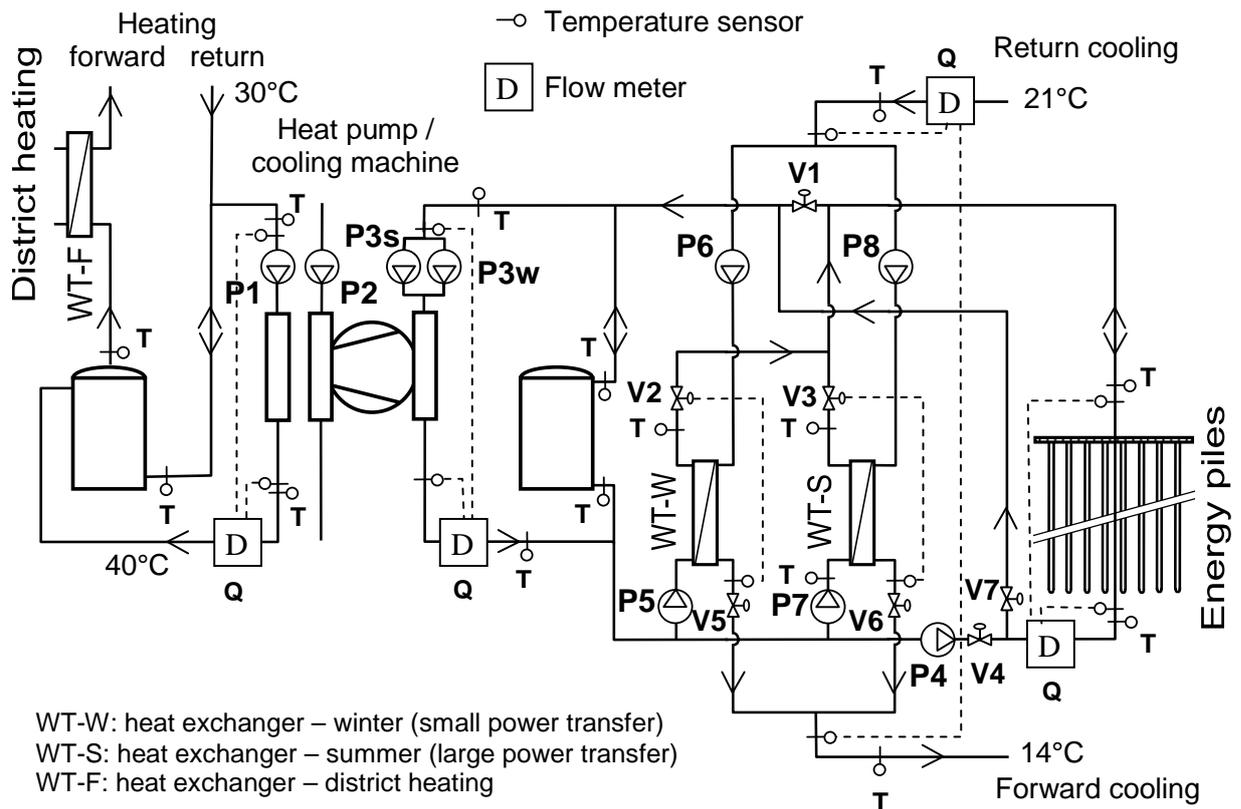


Figure 2: System layout and measurement points

Cooling energy is transferred in the pile system through a heat exchanger (either WT-W or WT-S). The forward fluid temperature of 14°C in the cooling distribution is controlled with a variable flow rate in the pile circuit, controlled with either valve V2 or V3. As flow rate cannot be decreased below a given value, a smaller heat exchanger (WT-W) takes over the large one (WT-S) when the fluid temperature in the pile circuit is too low (normally in winter), in order to create a large temperature difference through the heat exchanger.

The system operation mode is controlled by the on/off valves V1, V4 and V7. Heat extraction from the pile requires V1 and V4 open, V7 closed and P4 switched on. Geocooling or heat injection in the pile is achieved with V1 and V4 closed, V7 open and P4 switched off.

The pile system monitoring is performed with measurements of 15 fluid temperatures, 11 operation status for the circulation pumps and the heat pump, 5 heat meters including district heating contribution, 15 ground temperatures in four piles which were not used as energy pile and the outside air temperature. These measures are recorded by the building automation system every 5 minutes. Separate dataloggers are also installed to record the electric consumptions of the circulation pumps and the heat pump / cooling machine. The results of the monitoring campaign can be found in Pahud and Hubbuch (2007).

3 HEATING PRODUCTION

The heat pump is 4.4 m long, 2.1 m wide and 2.1 m high. The refrigerant fluid is R717 (ammonia), which requires the heat pump to be placed in a ventilated room maintained under a slight depression for security reason in case of leakage. The heat pump may operate at 25, 50, 75 or 100% of its nominal power. It is shown in figure 3.

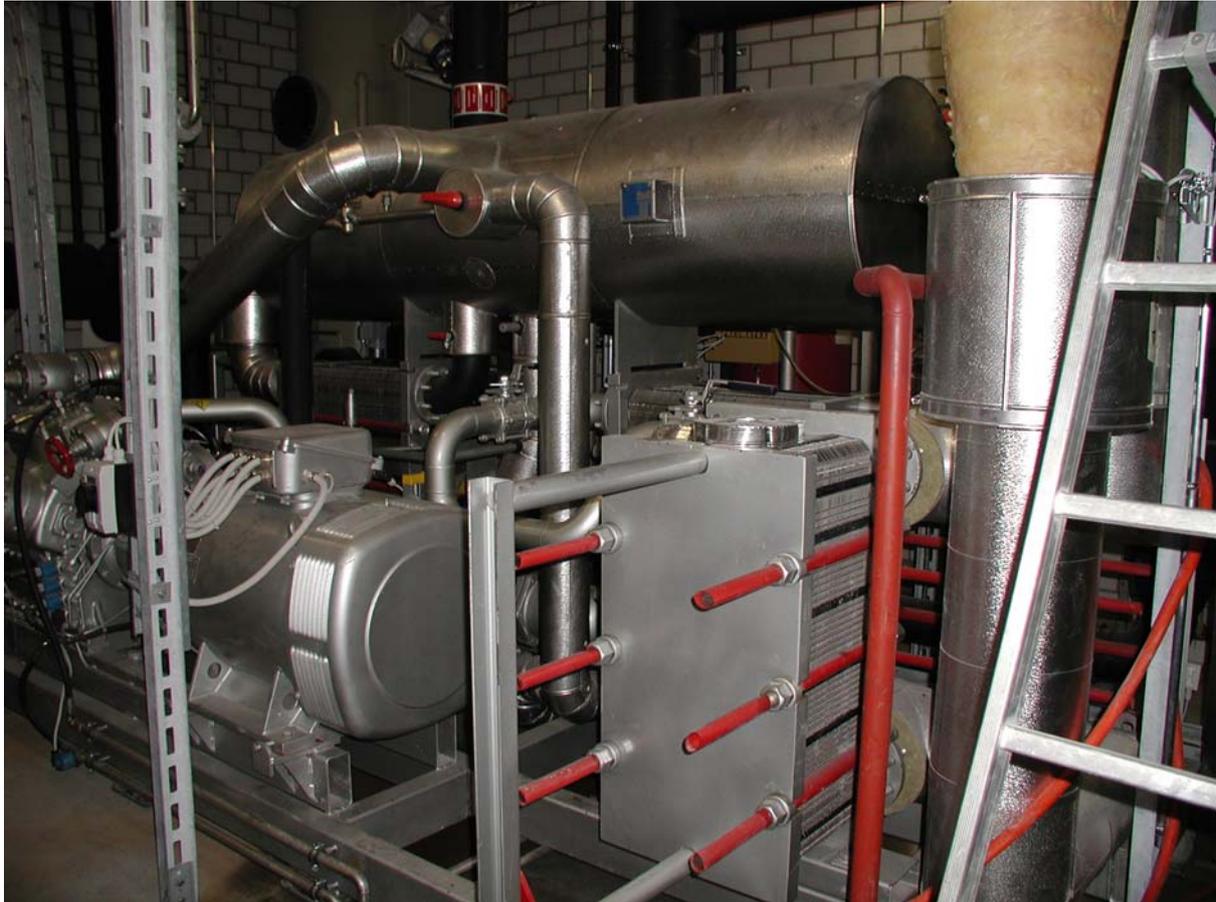


Figure 3: Ammonia heat pump of the Dock Midfield energy pile system

The measured monthly thermal performances of the heat pump are shown in figure 4 from October 2005 until September 2006.

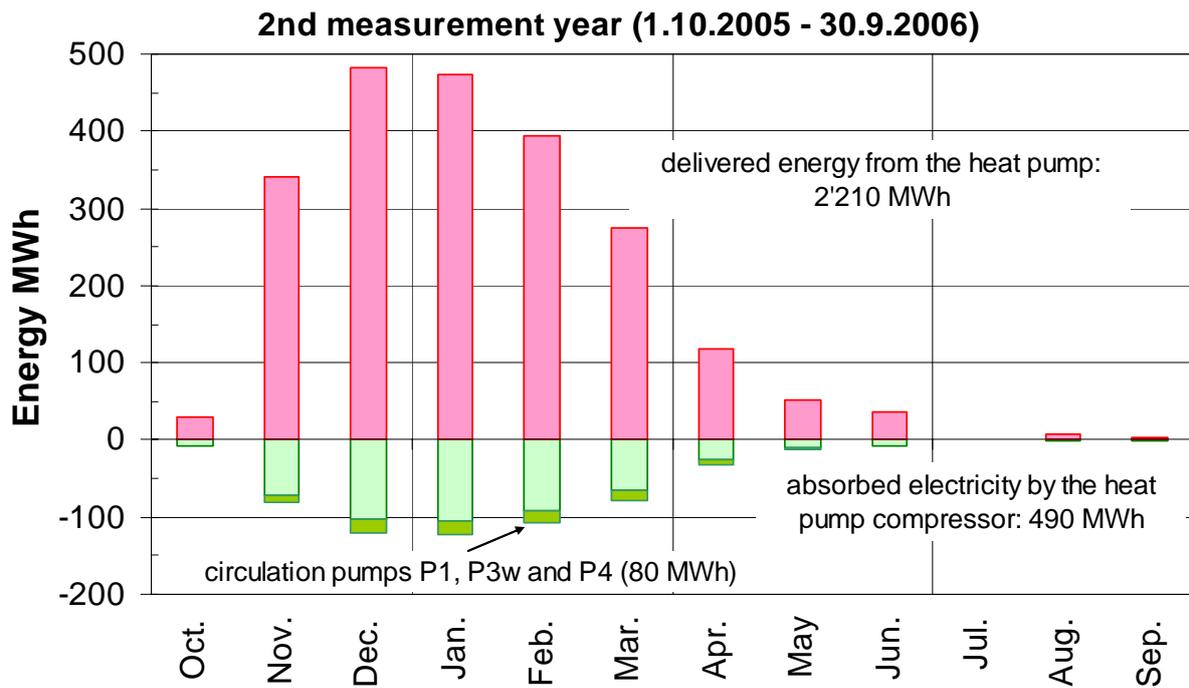


Figure 4: Monthly thermal performances of the heat pump

Heating energy delivered by the heat pump is measured to 2'210 MWh. With a district heating contribution of 810 MWh, the annual thermal energy is measured to 3'020 MWh. The annual thermal performance coefficient of the heat pump (COPA) is established to 3.9, including the electric energy for the circulation pumps P1 (condenser), P3w (evaporator) and P4 (energy piles). The mean annual temperature level of the outlet fluid from the heat pump condenser is 39°C and is rather constant throughout the heating period. The mean annual temperature level of the inlet fluid in the heat pump evaporator is established to 8.3°C. The lowest monthly value is observed in February with a value of 6.4°C.

The evolution of the distributed heating power is shown in figure 5, together with the classified values for winter 2005 – 2006.

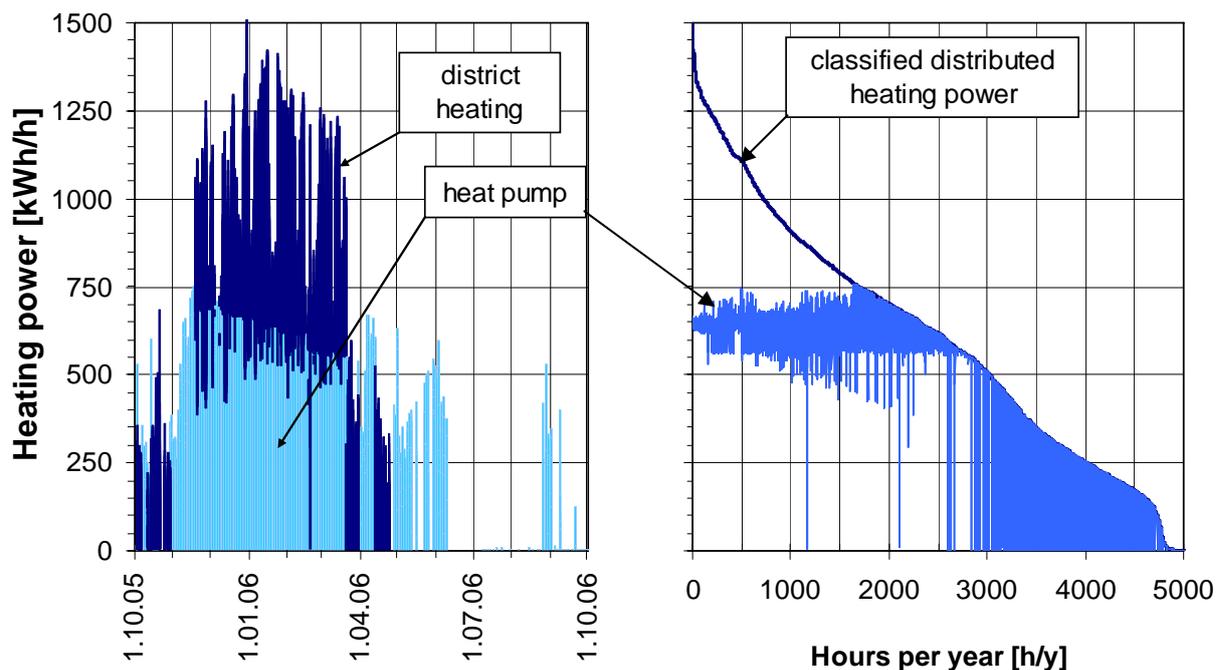


Figure 5: Thermal power delivered in the building by the pile system during winter 2005 - 2006

4 COOLING PRODUCTION

The measured monthly cooling energies of the cooling distribution network are shown in figure 6 from October 2005 until September 2006.

The electric energy for the circulation pumps and the cooling machine is measured to 90 MWh. The overall cooling efficiency, defined by the ratio between the delivered cooling energy and the electric energy used to operate the system for the cooling production, is established to 13. This large value is also due to the particularly high geocooling efficiency (61). The cooling machine efficiency, established to 2.7, is heavily penalized by the electric consumption of the circulation pumps. It represents more than 70% of the compressor electric consumption of the cooling machine.

The return fluid temperature from the cooling distribution network is rather constant throughout the summer and is measured to 17°C. This value is much lower than the expected 21°C. It considerably penalizes the geocooling production, which has to be compensated for by the cooling machine one.

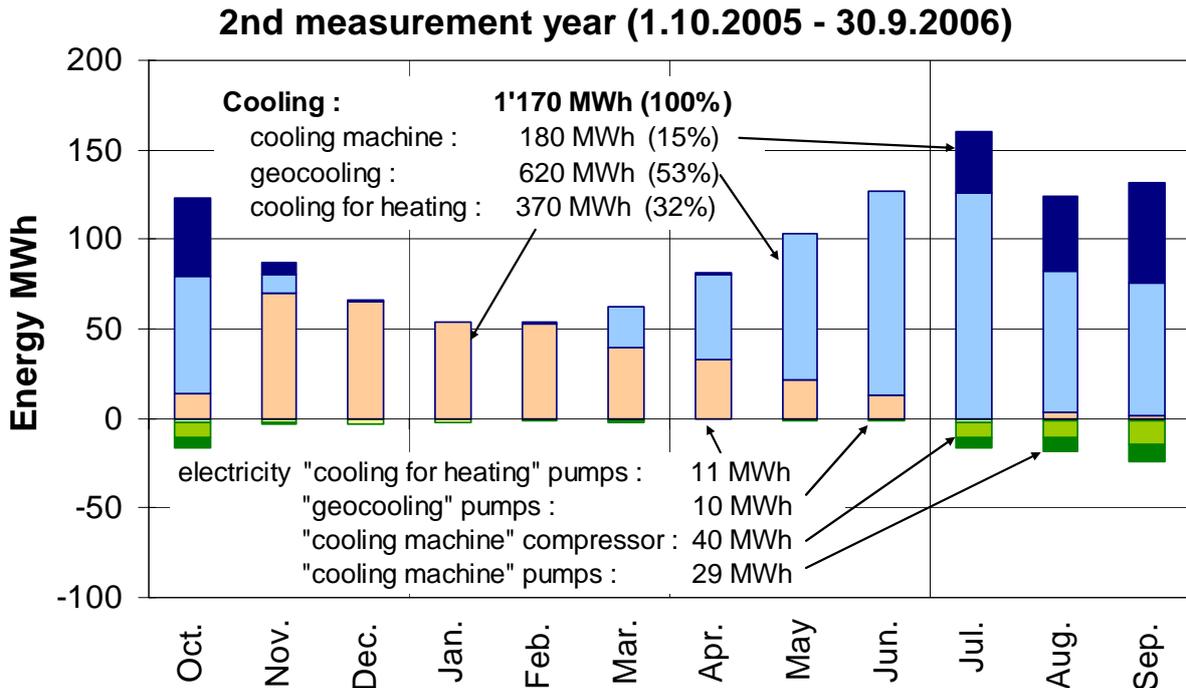


Figure 6: Monthly cooling energies delivered in the cooling distribution network

5 ENERGY PILES

In figure 7, monthly extracted and injected energies in the piles are shown. The injected energy is in fact the geocooling production. Measured to 620 MWh, it represents 41% of the 1'500 MWh extracted by the heat pump. Monthly temperature levels of the fluid temperature at the inlet and outlet of the pile circuit are also shown for the extraction and injection operation modes.

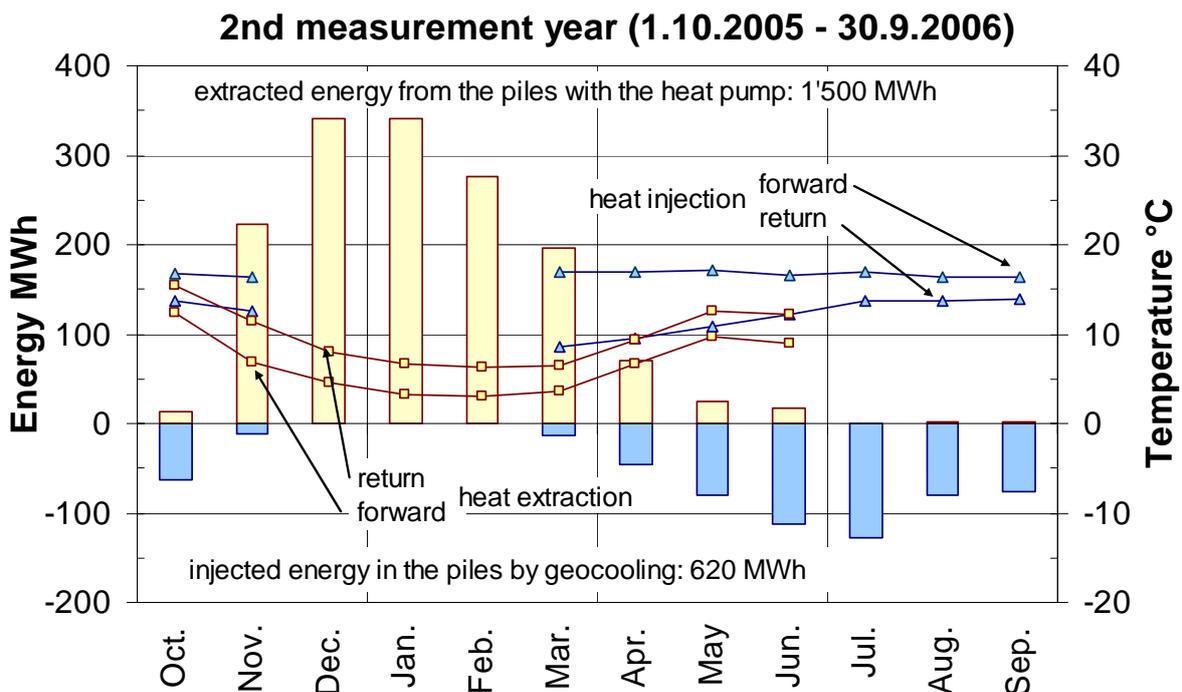


Figure 7: Monthly cooling energies delivered in the cooling distribution network

The ground temperatures are measured in a pile which is not used as an energy pile (see figure 8). The fluid temperature levels at the inlet and outlet of the pile flow circuit are now shown with daily values for the extraction and injection operation modes.

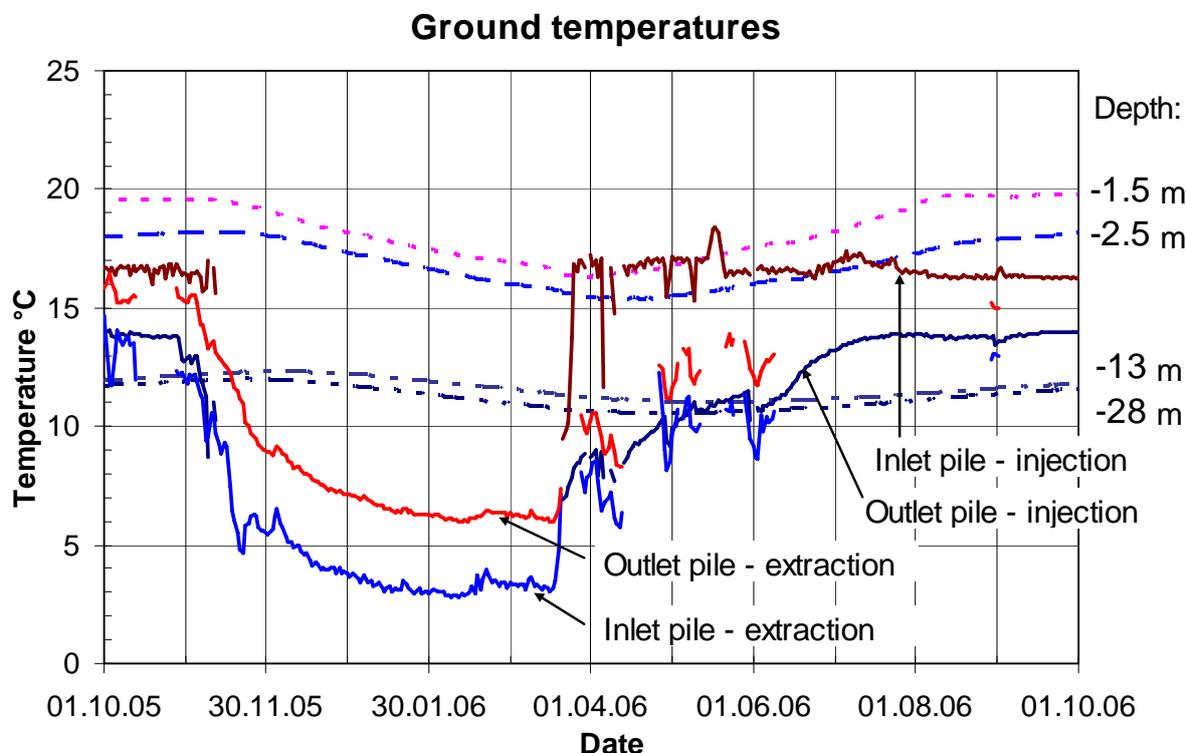


Figure 8: Ground temperatures at various depths. Daily temperature levels of the heat carrier fluid in the pile flow circuit are shown for both extraction and injection operation modes

The minimum inlet fluid temperature in the piles is measured to 2.4°C the first measurement year and 2.5°C the second one. The ground temperature, below the thermal influence of the surface, exhibits seasonal but small variations, due to the large ground volume involved.

6 SYSTEM HEAT BALANCE

The heat balance of the pile system is shown in figure 9. The measured values are compared to the design value established with PILESIM (Pahud 1998).

The measured values correspond astonishingly well to the predicted ones. The good accuracy of the simulated heating and cooling demands (Koschenz and Weber 1998) can be noticed. This confirms the pertinence of the design procedures adopted and the simulation tools used for the sizing of the system.

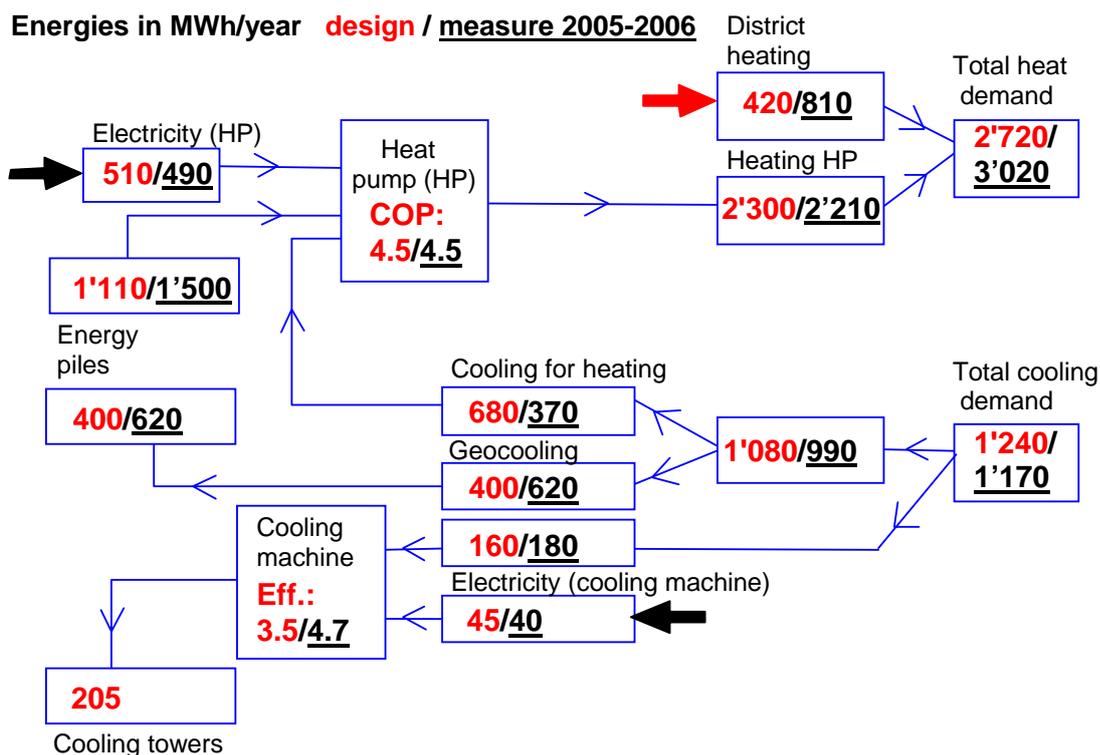


Figure 9: Pile system heat balance, comparison measured – predicted values with PILESIM

In table 2, a comparison of the design and measured thermal characteristics of the piles is shown.

Table 2: Key values associated with the thermal use of the piles; comparison design – measure 2005-2006

The values are referred to the active pile length		Design	Measurement
Pile heat extraction rate	maximum (W/m)	49	72 (+47%)
	average (W/m)		45
Pile annual heat extraction	(kWh/(m y))	135	183 (+36%)
Pile heat injection rate	maximum (W/m)	49	33 (-33%)
	average (W/m)		16
Pile annual heat extraction	(kWh/(m y))	48	74 (+54%)
Ratio injected over extracted		36%	41% (+14%)

The piles are actually used more intensively than expected, apart from the maximum heat injection rate, which is lower due to a low return fluid temperature from the cooling distribution. However the ground ratio is close enough to the design one, so that a long term operation of the system is guaranteed.

The thermal performance indexes of the pile system are shown in table 3. The overall system efficiency, defined by the ratio of the thermal energy delivered by the system (heating and cooling) over the total electric energy required to run it (all the circulation pumps and the heat pump / cooling machine), is established to 5.1.

Table 3: Annual thermal performance indexes related to the pile system for the second measurement year. The energy fraction is referred to the total heating and cooling energy supplied by the pile system

Performance index	Measured	Energy fraction
Annual heat pump performance coefficient	3.9	65%
“Cooling for heating” efficiency	33	11%
Geocooling efficiency	61	18%
Annual cooling machine efficiency	2.7	5%
Overall system efficiency	5.1	100%

7 PILESIM2 AND GEOCOOLING

Thanks to the detailed measurements of the system, the PILESIM program has been improved to better take into account geocooling calculation. PILESIM2 (Pahud 2007), the version 2 of PILESIM, has been developed in margin of this project and successfully calibrated to the measured thermal performances (Pahud and Hubbuch 2007).

The calibrated input data to PILESIM2 were used to analyze the geocooling energy sensitivity to the various design parameters. The two most important parameters are the temperature levels of the fluid in the cooling distribution and the heat transfer of the horizontal pipe connections between the piles. The heat transfer takes place between the pipes and the ground at the surface, whose temperature is influenced by the building itself. The lower the cooling forward fluid temperature is, the lesser the geocooling energy and the greater the negative influence of the heat transfer of the horizontal pipe connections are. These effects are shown in figure 10 for the case of Dock Midfield.

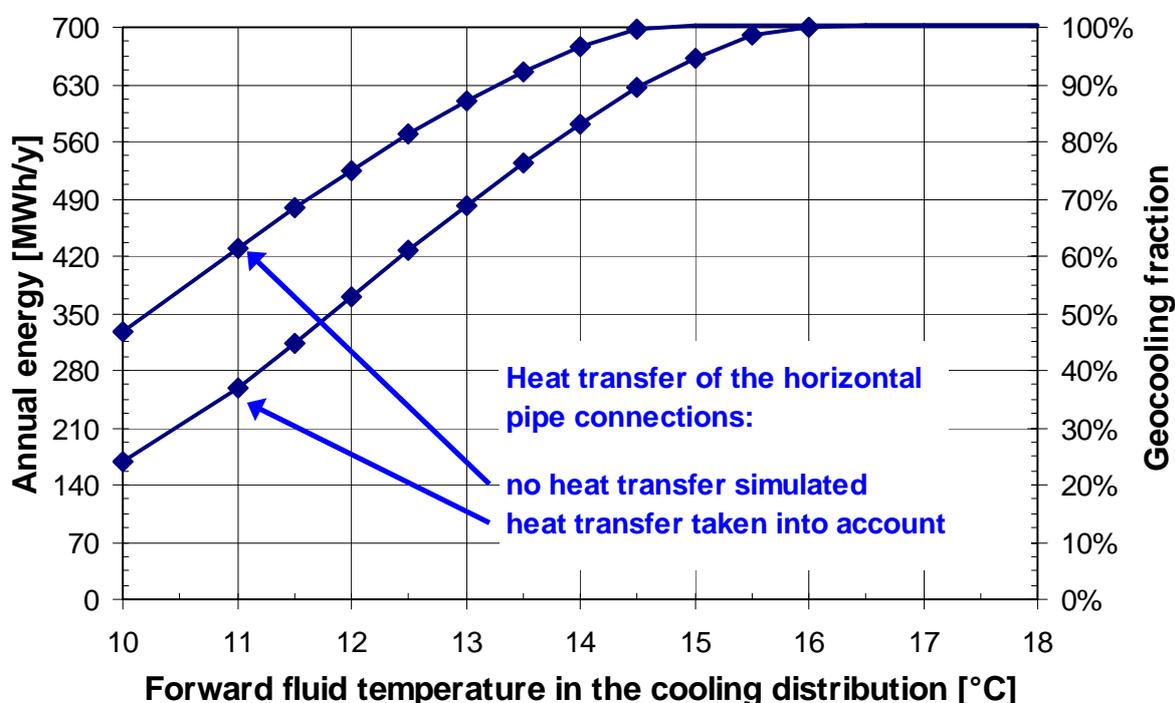


Figure 10: Sensitivity of the geocooling potential to the fluid temperature level in the cooling distribution and the importance of the heat transfer of the horizontal pipe connections with the ground

If cooling energy could be delivered at 16 – 17°C in the cooling distribution, with a return fluid temperature of 19 – 20°C, the totality of the cooling energy could be delivered by geocooling and the cooling machine would not be used. The global system efficiency would rise from 5.1 to 5.7.

8 ECONOMICAL ASPECTS

The investment for the use of the energy piles amounts to 670'000 €. The pile system provides a saving of 80'000 €, due to the non installation of cooling units in the luggage handling rooms (UNIQUE 2003). Relative to a conventional system, the major investment of the pile system is 590'000 €. On the basis of the measured energies, the cost of the purchased final energy and the maintenance cost, an economical comparison of the pile system with a conventional one is shown in table 4.

Table 4: Economical aspect of the pile system and comparison with a conventional system

System	energy piles	conventional	difference
Investment	670'000 €	80'000 €	+590'000 €
Annual cost			
capital	46'170 €	5'450 €	+40'720 €
maintenance	10'070 €	3'170 €	+6'900 €
energy	71'660 €	156'180 €	- 84'520 €
Total annual cost	127'900 €	164'800 €	- 36'900 €
Thermal energy cost	0.04 €/kWh	0.05 €/kWh	

Relative to a conventional system, the pile system supplementary investment is paid back in 8 years, if the interests of the invested capital is not taken into account.

9 CONCLUSION

The thermal performances of the pile system are very satisfactory. They are close to the design values. It confirms the rightness and necessity of the important effort invested in the design phase of the system. It included two thermal response tests, dynamic building simulations for the determination of the energy requirements and pile system thermal simulations.

Measurements were used to validate the development of PILESIM2, the version 2 of PILESIM. The new version better takes into account geocooling calculations. Calculations showed that the cooling machine would not be used if cooling energy can be distributed at 16 – 17°C instead of 14°C. The overall system efficiency, measured to 5.1, would rise to 5.7. This high efficiency is due to the geocooling efficiency, which has been measured to the exceptionally high value of 61. This highlights the correct sizing of the circulation pumps.

Economical evaluations confirm the good thermal performances of the system. The pile system is economically more convenient than a conventional system. This result is the consequence of the detailed and integrated approach used in the design phase. A special effort has been achieved to realise an optimal integration of the pile system in the global energy concept of the building.

10 ACKNOWLEDGEMENT

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